

On the finite element solution of helmholtz problems in anisotropic media

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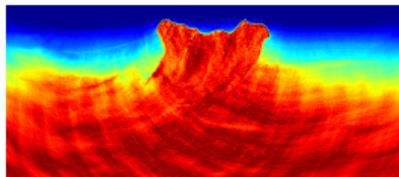
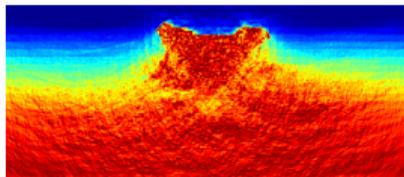
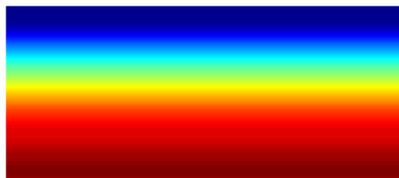
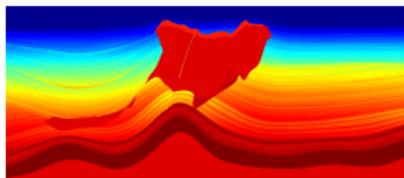
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LMA2S, DTIS, ONERA, 29 mars 2019



FWI using DG or FD

Same acoustic model of size 35×15 km. Exact same FWI algorithm (n iterations, frequencies, ...), **no initial information**.



Computations performed by Florian Faucher (Magique-3D)

The time harmonic anisotropic scalar wave equation

$$\begin{cases} \nabla \cdot (A(\mathbf{x})\nabla u(\mathbf{x})) + \mu(\mathbf{x})u(\mathbf{x}) = 0 & \text{in } \Omega \\ u(\mathbf{x}) = g(\mathbf{x}) & \text{on } \partial\Omega, \end{cases}$$

Anisotropies are handled inside the divergence operator

The matrix A is **symmetric**

$A = \lambda I$, for **isotropic** media

A and μ are often **piecewise constant**.

The domain Ω is 2D or 3D with boundary $\partial\Omega$.

Other boundary conditions can be as well considered

Motivation: Computations on very large domains

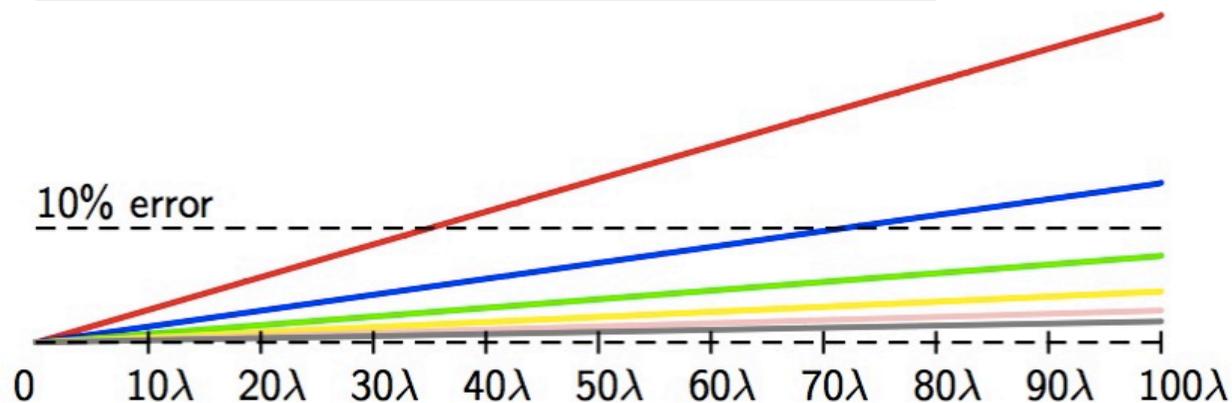
Ω is very large vs the wavelength

Need to augment the density of nodes to maintain a given level of accuracy

*Babuska, SA Sauter, Is the **pollution effect** of the FEM avoidable for the Helmholtz equation considering high wave numbers? SIAM Journal on numerical analysis, 1997 (cited 476 times)*

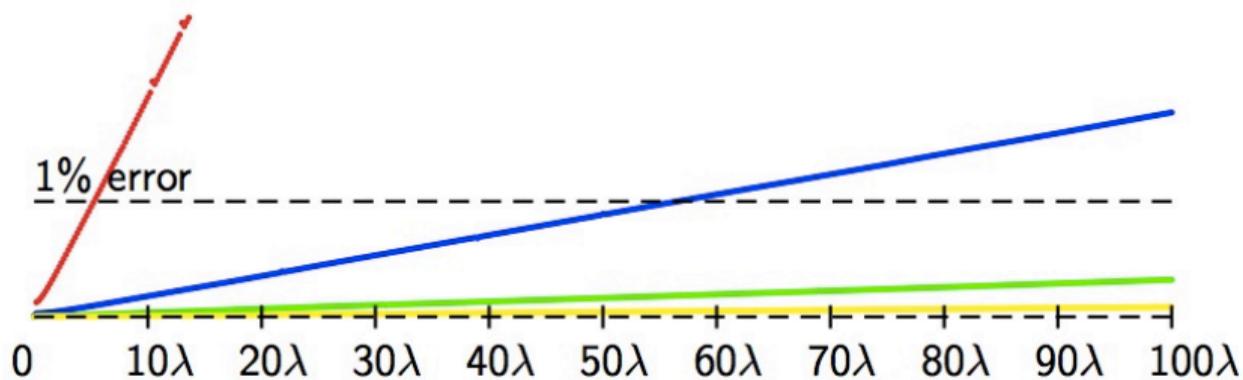
Error at every wavelength in \mathbb{P}_2 for 10, 12, 14, 16, 18 segments per λ

- 20 segments per λ , 4800 dof per λ^2
- 18 segments per λ , 3888 dof per λ^2
- 16 segments per λ , 3072 dof per λ^2
- 14 segments per λ , 2352 dof per λ^2
- 12 segments per λ , 1728 dof per λ^2
- 10 segments per λ , 1200 dof per λ^2



Error at every wavelength in \mathbb{P}_3 for 4, 6, 8, 10 segments per λ

- 10 segments per λ , 2000 dof per λ^2
- 8 segments per λ , 1280 dof per λ^2
- 6 segments per λ , 720 dof per λ^2
- 4 segments per λ , 320 dof per λ^2



Motivation: Computations on very large domains

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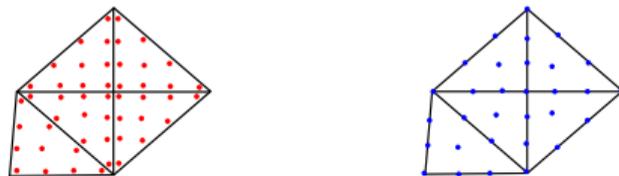
Exceed the storage capacities.

Discontinuous Galerkin methods do resist better to pollution effect

General setting

Studies show that DG weak inter-element continuity contributes to fight the pollution effect

But DG approximations imply to increase the number of nodes significantly



Lead to Trefftz methods

In particular, Ultra-Weak-Variational-Formulations proposed by B. Desprès and O. Cessenat.

Trefftz method: shape functions are solutions to the problem

Set on a single element T : Trefftz formulation reduces to the boundary of the element

Rewrite the IPDG and UWVF formulation in a different context

Classically, plane wave bases or Bessel functions inside each element.

Here we use an **auxiliary method** to compute local solutions.

We call these methods

BEM-STDG

FEM-STDG

FD-STDG

Plane-wave-STDG

BEM-UWVF

FEM-UWVF

FD-UWVF

Plane-wave-UWVF

General setting

For isotropic media

Boundary Integral Equations (BIE) lead to less pollution effect than FEMs

Recently, Hofreither et al. (2015) have proposed a FEM in which local shape functions are obtained on the basis of a BIE.

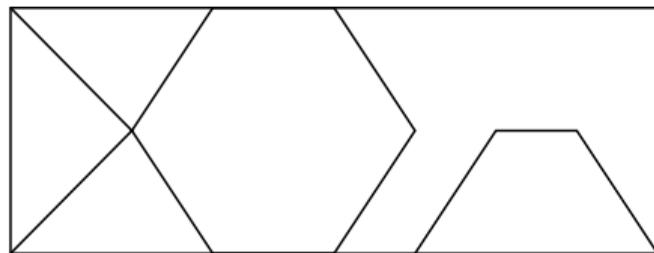
In the same spirit, we propose a DG method using local shape solutions to the Helmholtz problem that are matched at the interface of the mesh thanks to the Dirichlet-to-Neumann (DtN) operator which is computed with a BIE.

For anisotropic media

Very precise **Finite Element Method** to reproduce the BIE

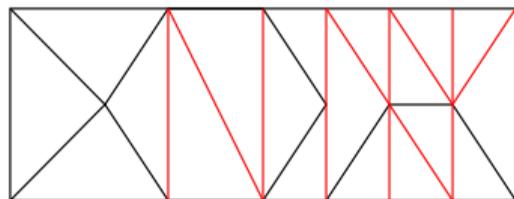
Can also handle strongly heterogeneous media

The mesh

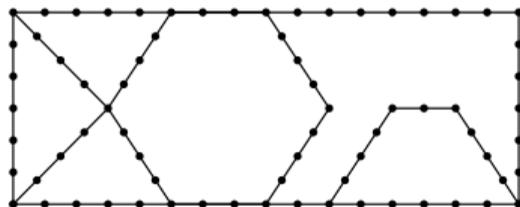


A smart finite element method

The mesh



A classical finite element mesh



A smart finite element mesh

Trial and test functions

Trial and test functions are solutions to the Helmholtz equation **in each element**

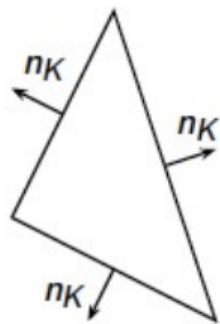
$$\operatorname{div}\left(A_K \nabla u_K(\mathbf{x})\right) + \mu_K u_K(\mathbf{x}) = 0 \text{ in } K$$

u_K is uniquely defined by its Dirichlet trace if K is small enough (**geometrical criterion**)

$$u_K \in H^{1/2}(\partial K)$$

The discrete variational space is then obtained by considering a discrete trace space

u_K is \mathbb{P}_r -continuous on ∂K .



Trial and test functions

Trial and test functions are solutions to the Helmholtz equation **in each element**

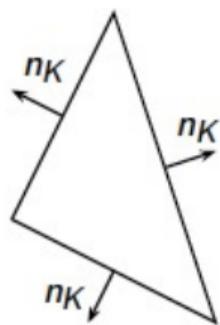
$$\operatorname{div}\left(A_K \nabla u_K(\mathbf{x})\right) + \mu_K u_K(\mathbf{x}) = 0 \text{ in } K$$

u_K is uniquely defined by its Robin trace

$$A_k \nabla u_K \cdot n_K + i\eta u_K \in H^{-1/2}(\partial K)$$

The discrete variational space is then obtained by considering a discrete trace space

$A_k \nabla u_K \cdot n_K + i\eta u_K$ is \mathbb{P}_r -discontinuous on ∂K .



The reciprocity principle for anisotropic media

Since u and v are solutions of the anisotropic Helmholtz equation on each element K .

$$\int_{\partial K} (A\nabla u) \cdot n v = \int_K (A\nabla u) \cdot \nabla v - \kappa^2 uv = \int_{\partial K} u \cdot n(A\nabla v) \quad (1)$$

The reciprocity principle is the main ingredient of any Trefftz method

$$\int_{\partial K} uq - pv = 0$$

Denoting by

$$p = (A\nabla u) \cdot n \quad q = (A\nabla v) \cdot n$$

This expression is the main ingredient of all the Trefftz formulation.

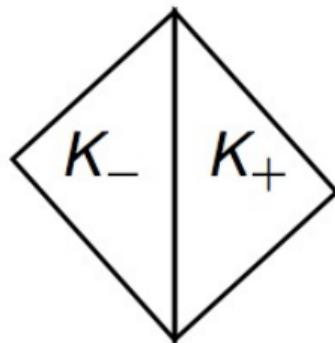
Symmetric Trefftz Variational Formulation

Summing over all the elements

$$0 = \sum_K \int_{\partial K} uq - pv ds_x$$

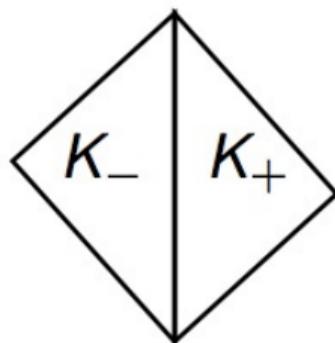
with the collection of interior edges Γ and $\partial\Omega$ the boundary of the domain

$$\left\{ \begin{array}{l} 0 = \int_{\Gamma} u_+ q_+ + u_- q_- - p_+ v_+ + p_- v_- ds_x \\ + \int_{\partial\Omega} uq - pv ds_x \end{array} \right.$$



Symmetric Trefftz Variational Formulation

$$\begin{cases} 0 = \int_{\Gamma} u_+ q_+ + u_- q_- - p_+ v_+ + p_- v_- ds_x \\ + \int_{\partial\Omega} uq - pv ds_x \end{cases}$$



The exact solution satisfies $u_+ = u_-$ and $p_+ = -p_-$ on Γ

$$\begin{cases} 0 = \int_{\Gamma} u_- q_+ + u_+ q_- + p_- v_+ + p_+ v_- ds_x \\ + \int_{\partial\Omega} uq - pv ds_x \end{cases}$$

and $u = g$ on $\partial\Omega$

$$\underbrace{\int_{\Gamma} u_- q_+ + u_+ q_- + p_- v_+ + p_+ v_- ds_x - \int_{\partial\Omega} pv + uq ds_x}_{a(u,p;v,q)} = \underbrace{-2 \int_{\partial\Omega} gq ds_x}_{\ell_2(v)}$$

The symmetric variational formulation

Adding the penalization terms ($[u] = 0$ on Γ and $u = g$ on $\partial\Omega$):

$$\underbrace{\int_{\Gamma} \alpha [u][v] + \int_{\partial\Omega} \alpha uv}_{b(u,p;v,q)} = \underbrace{\int_{\partial\Omega} \alpha g_D v}_{\ell_2(v)}$$

This leads to the Trefftz-DG formulation

$$a(u, p; v, q) + b(u, p; v, q) = \ell_1(q) + \ell_2(v).$$

Why **the symmetry** is important ?

for the linear algebra solver: it needs less memory

it has been observed that BIE methods are more stable.

Now, the unknowns are u and $p = A\nabla u \cdot \mathbf{n}$ on each face of the mesh. One may be removed.

The DtN operator

Let

$u_K(\mathbf{x})$ be given on ∂K .

The Neumann trace

$$p_K = A_K \nabla u_K \cdot \mathbf{n}_K \text{ on } \partial K$$

may then be deduced thanks to the Dirichlet-to-Neumann operator

$$DtN : \begin{cases} H^{\frac{1}{2}}(\partial K) \longrightarrow H^{-\frac{1}{2}}(\partial K) \\ u_K \longmapsto p_K \end{cases}$$

and we end up with a system involving unknowns defined on the boundary of each element.

The problem to be addressed: compute the DtN operator

The DtN operator approximation: include an auxiliary numerical method

We can think about different methods for **isotropic media** like:

finite element/finite difference method based on the velocity/pressure formulation

Boundary element method

Why BEM? They do resist very well to pollution effect

The secondary numerical method: BEM

$$\frac{V_K p_K}{\lambda_K} = \frac{M_K u_K}{2} - N_K u_K$$

u_K is approximated by a \mathbb{P}_r -continuous function

p_K is approximated by a $\mathbb{P}_{r'}$ -discontinuous function

V_K and N_K are the single layer and double layer operators.

$$\left\{ \begin{array}{l} (M_K u_K, q_k)_{\partial K} = \int_{\partial K} u_K(\mathbf{x}) q_K(\mathbf{x}) ds_{\mathbf{x}}, \\ (V_K p_K, q_k)_{\partial K} = \int_{\partial K} \int_{\partial K} p_K(\mathbf{x}) G_K(\mathbf{x} - \mathbf{y}) q_K(\mathbf{y}) ds_{\mathbf{x}} ds_{\mathbf{y}}, \\ (N_K u_K, q_k)_{\partial K} = \int_{\partial K} \int_{\partial K} p_K(\mathbf{x}) \frac{\partial G_K}{\partial \mathbf{n}_{\mathbf{y}}}(\mathbf{x} - \mathbf{y}) q_K(\mathbf{y}) ds_{\mathbf{x}} ds_{\mathbf{y}} \end{array} \right.$$

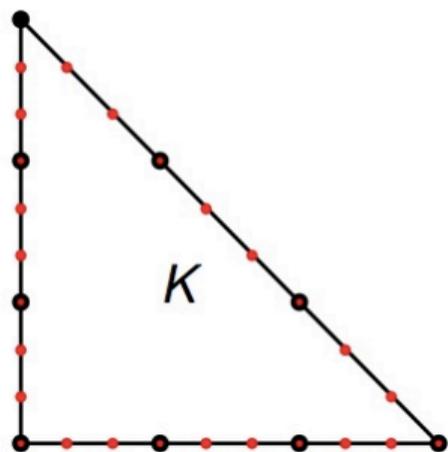
with

$$G(\mathbf{x}) = \frac{\exp(ik_K \|\mathbf{x}\|)}{4\pi \|\mathbf{x}\|} \text{ with } k_K = \sqrt{\frac{\mu_K}{\lambda_K}}$$

The boundary element method

u_K is approximated by a \mathbb{P}_r -continuous function

p_K is approximated by a $\mathbb{P}_{r'}$ -**dis**continuous function



- geometric nodes for p_K
- geometric nodes for u_K

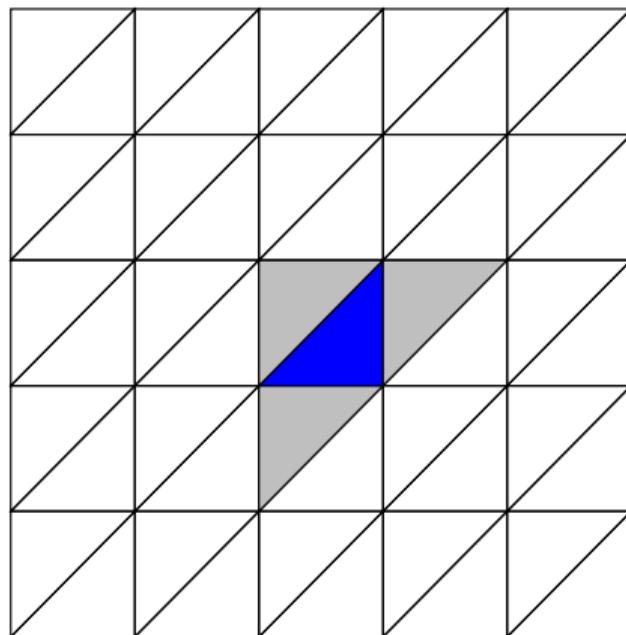
We can use different meshes for u_K and p_K .

Idea: the Neumann trace must be computed accurately

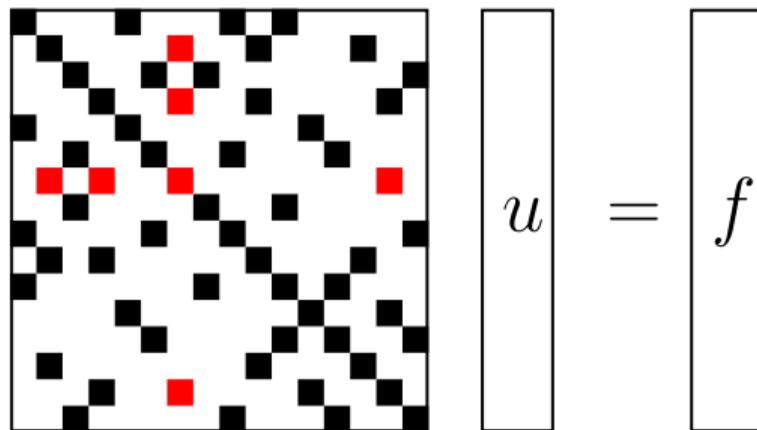
Remark: p_K is discontinuous, only at the geometric singularities.

The skeleton of the matrix

Connection of the elements

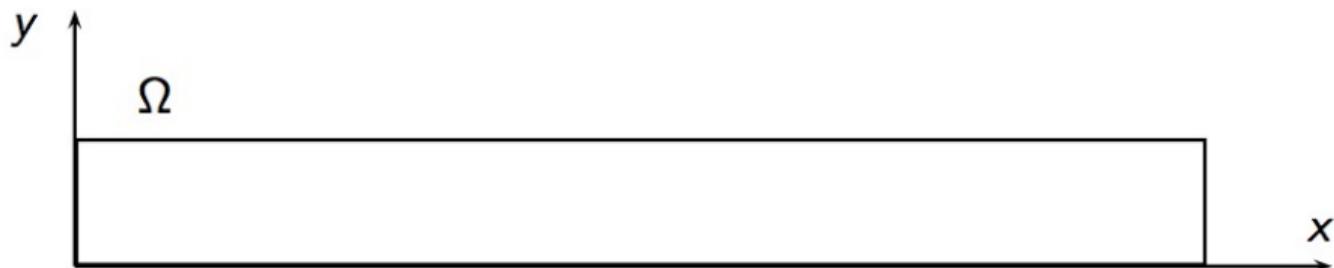


The final formulation


$$u = f$$

Symmetric block sparse matrix
full small blocks
really adapted to GMRES Solver

A numerical simulation



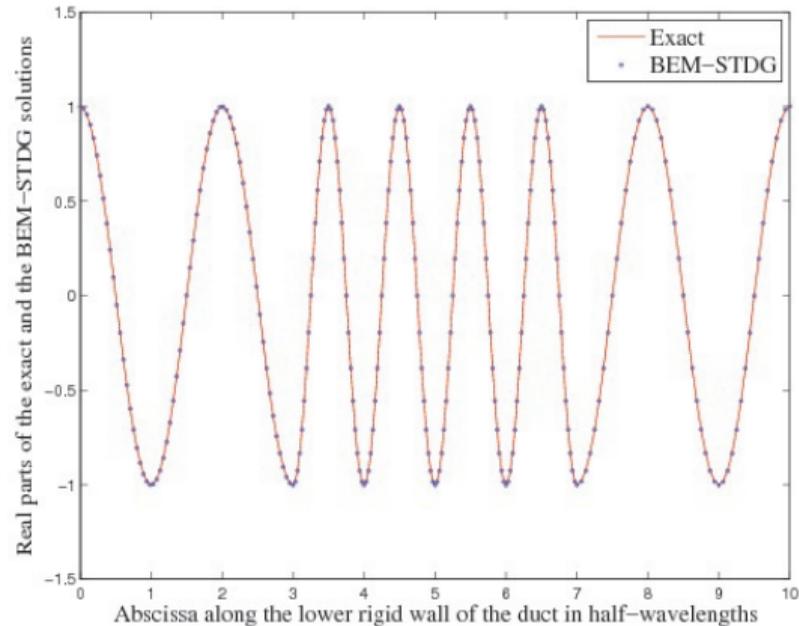
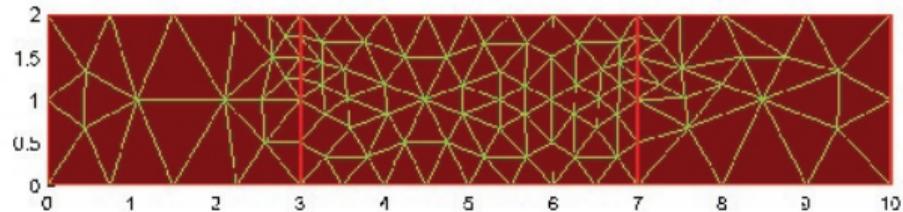
$$\left\{ \begin{array}{ll} \Delta u(\mathbf{x}) + k^2 u(\mathbf{x}) = 0 & \text{in } \Omega \\ u(\mathbf{x}) = 1 & \text{at } x = 0, \\ \frac{\partial u}{\partial n}(\mathbf{x}) = 0 & \text{at } x = N\lambda \\ \frac{\partial u}{\partial n}(\mathbf{x}) + iku(\mathbf{x}) = 0 & \text{at } y = 0 \text{ and } N\lambda \end{array} \right. \quad (2)$$

Poly degree	nodes per λ	Method	Error at 175λ for \mathbb{P}_2 Error at 500λ for \mathbb{P}_3
$m = 2$	12	IPDG	72 %
		BEM-STDG	22 %
	16	IPDG	67 %
		BEM-STDG	5.6 %
	24	IPDG	13 %
		BEM-STDG	0.8 %
$m = 3$	12	IPDG	19 %
		BEM-STDG	1.6 %
	18	IPDG	1.7 %
		BEM-STDG	0.1 %
	24	IPDG	0.3 %
		BEM-STDG	0.02 %

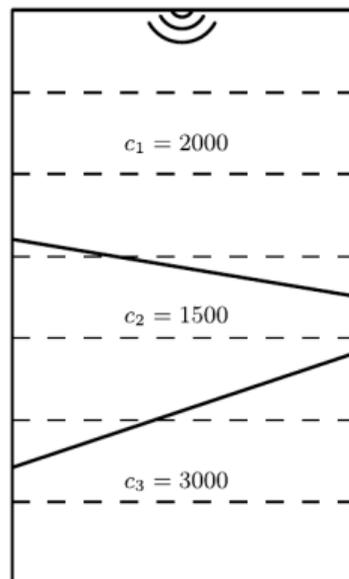
Degree	Density (nodes/ λ)	Method	Condition number		CPU time
			50 λ	500 λ	500 λ
$m = 2$	12	IPDG	$8.8 \cdot 10^{10}$	$4.7 \cdot 10^{11}$	2.54
		BEM-STDG	$6.06 \cdot 10^7$	$1.00 \cdot 10^8$	4.76
	24	IPDG	$1.2 \cdot 10^{12}$	$2.76 \cdot 10^{12}$	19.03
		BEM-STDG	$5.96 \cdot 10^8$	$9.42 \cdot 10^9$	8.5
$m = 3$	12	IPDG	$4.2 \cdot 10^{11}$	$8.9 \cdot 10^{11}$	2.13
		BEM-STDG	$2.1 \cdot 10^8$	$1.5 \cdot 10^9$	4.75
	24	IPDG	$2.0 \cdot 10^{12}$	$6.2 \cdot 10^{13}$	20.81
		BEM-STDG	$9.52 \cdot 10^8$	$8.07 \cdot 10^{10}$	8.4
$m = 4$	8	IPDG	$1.43 \cdot 10^{11}$	$3.78 \cdot 10^{11}$	0.66
		BEM-STDG	$1.13 \cdot 10^8$	$1.08 \cdot 10^8$	3.89
	24	IPDG	$2.38 \cdot 10^{12}$	$2.41 \cdot 10^{14}$	17.91
		BEM-STDG	$1.7 \cdot 10^9$	$1.7 \cdot 10^{11}$	8.41

Condition number and CPU time for h p refinements

Case of an unstructured mesh

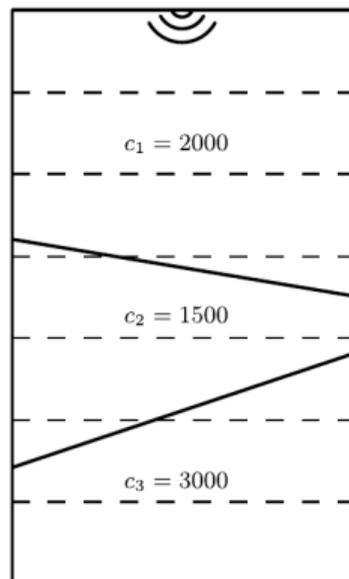


Case of an unstructured mesh of an heterogenous medium

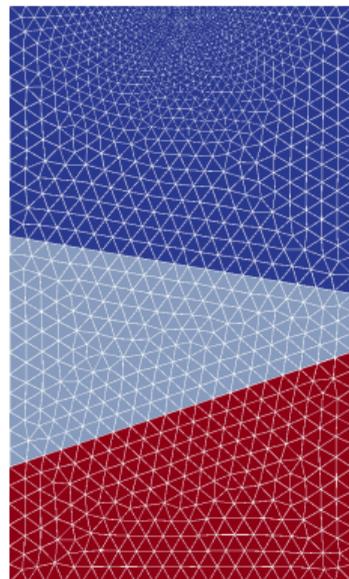


Configuration

Case of an unstructured mesh of an heterogenous medium

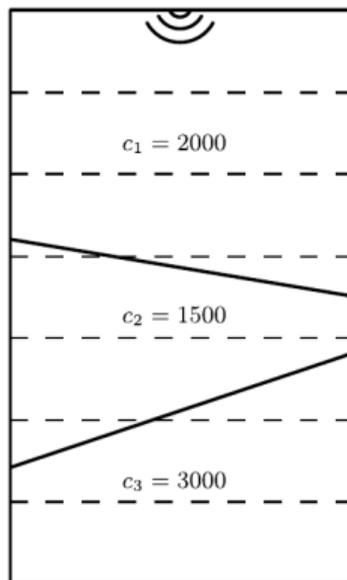


Configuration

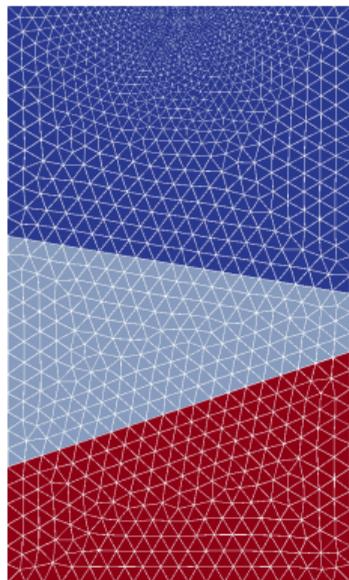


Mesh

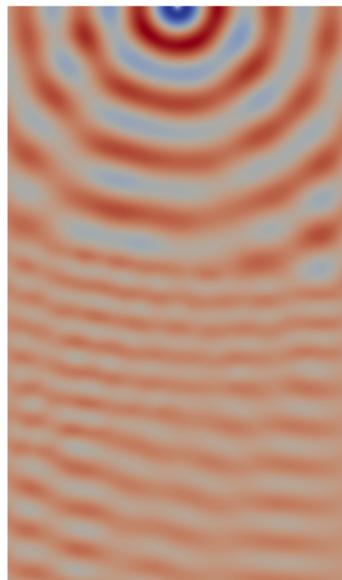
Case of an unstructured mesh of an heterogenous medium



Configuration

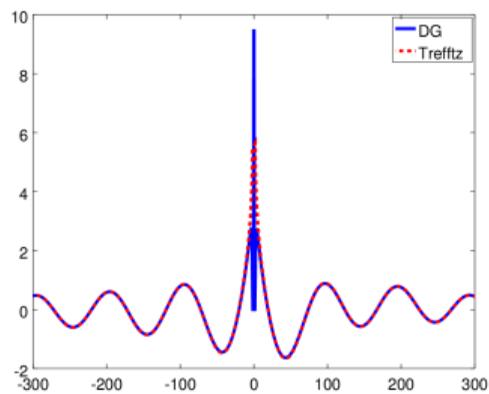


Mesh

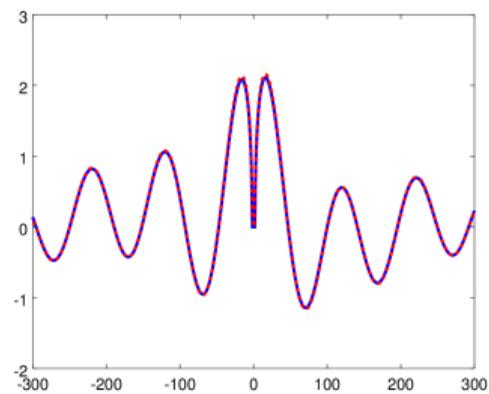


DG Solution
(Imaginary part)

Case of an unstructured mesh of an heterogenous medium



Real part



Imaginary part

The anisotropic Ultra Weak Variational method

The basis of the reciprocity principle is the reciprocity principle

$$\sum_K \int_{\partial K} uq - pv = 0$$

and the identity

$$uq - pv = \frac{(p + i\eta u)(q - i\eta v) - (p - i\eta u)(q + i\eta v)}{2i\eta}$$

The choice of η

is well known for isotropic and homogenous media $\eta = k$

has not been defined correctly for heterogeneous media

has not yet been defined for heterogeneous anisotropic media

The trial and test functions

We denote by

$$\left\{ \begin{array}{l} x_T = \frac{u_T}{2} + \frac{p_T}{2i\eta_T}, \\ \tilde{x}_T = \frac{u_T}{2} - \frac{p_T}{2i\eta_T}, \\ y_T = \frac{v_T}{2} + \frac{q_T}{2i\eta_T}, \\ \tilde{y}_T = \frac{v_T}{2} - \frac{q_T}{2i\eta_T}. \end{array} \right.$$

The **reciprocity principle**:

$$\int_{\partial T} x_T \tilde{y}_T \eta_T ds = \int_{\partial K} y_T \tilde{x}_T \eta_T ds$$

x_T is a trial function

Reflexion transmission between two media

$$\begin{array}{ccc} \nabla \cdot (A_T \nabla u_T) - \mu_T^2 u_T = 0 & & \nabla \cdot (A_L \nabla u_L) - \mu_L^2 u_L = 0 \\ & p_T \neq -p_L & \\ & \leftarrow n_L \quad n_T \rightarrow & \\ & u_T \neq u_L & \\ \text{media 1} & & \text{media 2} \end{array}$$

We consider a plane wave orthogonal to the boundary

$$\begin{cases} u_T(x) = I_T^{in} \exp(ik_T x_1) + I_T^{out} \exp(-ik_T x_1) & x_1 > 0, \\ u_L(x) = I_L^{in} \exp(-ik_L x_1) + I_L^{out} \exp(ik_L x_1) & x_1 < 0 \end{cases}$$

Link with the choice of η for the UWVF method

$$\left\{ \begin{array}{l} I_T^{in} = \frac{u_T}{2} + \frac{p_T}{2i\eta_T} \\ I_T^{out} = \frac{u_T}{2} - \frac{p_T}{2i\eta_T} \\ I_L^{in} = \frac{u_L}{2} + \frac{p_L}{2i\eta_L} \\ I_L^{out} = \frac{u_L}{2} - \frac{p_L}{2i\eta_L} \end{array} \right.$$

with η given by

$$\left\{ \begin{array}{l} \eta_T = k_T \sqrt{\mathbf{n} \cdot (A^T \mathbf{n})} \\ \eta_L = k_L \sqrt{\mathbf{n} \cdot (A^L \mathbf{n})} \end{array} \right.$$

This will be our choice of η

Transmission condition between two media

For the plane wave solution

$$I_T^{out} = R_{TL} I_T^{in} + T_{LT} I_L^{in},$$

$$I_L^{out} = R_{LT} I_L^{in} + T_{TL} I_T^{in}.$$

with

$$\left\{ \begin{array}{ll} R_{TL} = \frac{\eta_T - \eta_L}{\eta_L + \eta_T} & R_{LT} = \frac{\eta_L - \eta_T}{\eta_T + \eta_L} \\ T_{TL} = \frac{2\eta_T}{\eta_L + \eta_T} & T_{LT} = \frac{2\eta_L}{\eta_L + \eta_T} \end{array} \right.$$

The Transmission Condition between two media

This last expression is rephrased in terms of the x_T variables

$$\begin{cases} \tilde{x}_T = R_T x_T + T_{LT} x_L, \\ \tilde{x}_L = R_L x_L + T_{TL} x_T. \end{cases}$$

and in terms of u and p

$$\begin{cases} -p_T + i\eta_L u_T = p_L + i\eta_L u_L, \\ -p_L + i\eta_T u_L = p_T + i\eta_T u_T. \end{cases}$$

This is rather similar to an **upwind flux**.

The boundary conditions

$$\begin{cases} u = g_D, & \text{(Dirichlet condition)} \\ p = g_N & \text{(Neumann condition)} \end{cases}$$

can be rewritten in terms of incoming and outgoing waves

$$-\frac{1}{2i\eta} (A\nabla u \cdot \mathbf{n} - i\eta u) = \frac{Q}{2i\eta} (A\nabla u \cdot \mathbf{n} + i\eta u) + g$$

with Q given here by

$$\begin{cases} Q = -1, & g = g_D, & \text{on } \partial\Omega_D, \\ Q = +1, & g = -g_N/i\eta, & \text{on } \partial\Omega_N, \end{cases}$$

The boundary conditions

$$\begin{cases} u = g_D, & \text{(Dirichlet condition)} \\ p = g_N & \text{(Neumann condition)} \end{cases}$$

can be rewritten in terms of incoming and outgoing waves

$$\tilde{x}_T = Qx_T + g$$

with Q given here by

$$\begin{cases} Q = -1, & g = g_D, & \text{on } \partial\Omega_D, \\ Q = +1, & g = -g_N/i\eta, & \text{on } \partial\Omega_N, \end{cases}$$

UWVF formulation with outgoing and incoming waves

The starting point is the reciprocity principle

$$\int_{\partial T} x_T \tilde{y}_T \eta_T ds = \int_{\partial T} \tilde{x}_T y_T \eta_T ds$$

UWVF formulation with outgoing and incoming waves

The starting point is the reciprocity principle

$$\int_{\partial T} x_T \tilde{y}_T \eta_T ds = \sum_{F_T \in \mathcal{F}_\partial} \int_{F_T} \tilde{x}_T y_T \eta_T ds + \sum_{F_{TL} \in \mathcal{F}_I} \int_{F_{TL}} y_T \tilde{x}_T \eta_T ds$$

where we have decomposed the boundary into two parts

the edges shared \mathcal{F}_I with another element L

the exterior edges \mathcal{F}_∂

UWVF formulation with outgoing and incoming waves

The starting point is the reciprocity principle

$$\int_{\partial T} x_T \tilde{y}_T \eta_T ds = \sum_{F_T \in \mathcal{F}_\partial} \int_{F_T} \tilde{x}_T y_T \eta_T ds + \sum_{F_{TL} \in \mathcal{F}_I} \int_{F_{TL}} T_{TL} x_{LYT} \eta_T ds + \sum_{F_{TL} \in \mathcal{F}_I} \int_{F_{TL}} R_{TL} x_T y_T \eta_T ds$$

For the edges of the boundary, we replace \tilde{x}_T by

$$\tilde{x}_T = Qx_T + g$$

UWVF formulation with outgoing and incoming waves

The starting point is the reciprocity principle

$$\int_{\partial T} x_T \tilde{y}_T \eta_T ds = \sum_{F_T \in \mathcal{F}_\partial} \int_{F_T} (Q_T x_T + g) y_T \eta_T ds + \sum_{F_{TL} \in \mathcal{F}_I} \int_{F_{TL}} T_{TL} x_L y_T \eta_T ds + \sum_{F_{TL} \in \mathcal{F}_I} \int_{F_{TL}} R_{TL} x_T y_T \eta_T ds$$

For the edges of the boundary, we replace \tilde{x}_T by

$$\tilde{x}_T = Q x_T + g$$

For the interior edges, we replace \tilde{x}_T by

$$\tilde{x}_T = R_{TL} x_T + T_{LT} x_L.$$

It remains to understand what is the $\tilde{\cdot}$ operator

The incoming to outgoing operator

Given $x_T \in L^2(\partial K)$, we consider the solution of

$$\left\{ \begin{array}{l} \text{Find } u \in H^1(K) \text{ tel que } \nabla \cdot (A \nabla u) + \mu u = 0 \quad \text{dans } T \\ \frac{u_T}{2} - \frac{A \nabla u_T \cdot \mathbf{n}_T}{2i\eta_T} = x_T \quad \text{sur } \partial T \end{array} \right.$$

$$\tilde{x}_T = \frac{u_T}{2} + \frac{p_T}{2i\eta_T} = u_T - \left(\frac{u_T}{2} - \frac{p_T}{2i\eta_T} \right) = u_T - x_T.$$

No need to compute p_T to get \tilde{x}_T .

The incoming to outgoing operator is a **unitary operator**

$$\left\{ \begin{array}{l} \tilde{\cdot}_T : L^2(\partial T) \longrightarrow L^2(\partial T) \\ x_T \longmapsto \tilde{x}_T \end{array} \right.$$

$$\begin{cases} \nabla \times \frac{1}{\mu} \nabla \times \mathbf{E} - \varepsilon k^2 \mathbf{E} = 0 & \text{in } \Omega \\ \mathbf{n} \times \left(\frac{1}{\mu} \nabla \times \mathbf{E} \right) - Z \mathbf{n} \times (\mathbf{E} \times \mathbf{n}) = \mathbf{g}_R & \text{on } \partial\Omega_R \\ \mathbf{n} \times (\mathbf{E} \times \mathbf{n}) = \mathbf{g}_D & \text{on } \partial\Omega_D \end{cases}$$

Problem well posed.

$$\mathbf{E} \in H(\text{curl}, \Omega)$$

$\varepsilon, \mu > 0$, piece-wise
constant

$$\mathbf{g}_D, \mathbf{g}_R \in L_t^2(\partial\Omega)$$

$$\text{Im}(Z) > 0$$

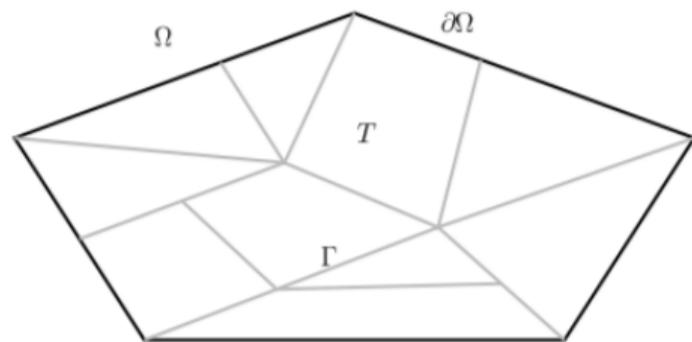
$$k = \frac{\omega}{c}$$

The symmetric DG Trefftz formulation

The DG formulation mesh

$$\bar{\Omega} = \bigcup_{T \in \mathcal{T}} \bar{T}, \quad T \cap K = \emptyset \quad \text{if} \quad T \neq K$$

$$\Gamma = \bigcup_{F \in \mathcal{F}_I} F, \quad \partial\Omega = \bigcup_{F \in \mathcal{F}_\partial} F$$



The symmetric DG Trefftz formulation

The basis function space

$$X_T = \left\{ \boldsymbol{\omega} \in H(\text{curl}, T); \quad \nabla \times \frac{1}{\mu_T} \nabla \times \boldsymbol{\omega} - \varepsilon_T k_T^2 \boldsymbol{\omega} = 0 \quad \text{in } T, \right. \\ \left. \mathbf{n} \times (\boldsymbol{\omega}|_{\partial T} \times \mathbf{n}), \quad \mathbf{n} \times \left(\frac{1}{\mu} \nabla \boldsymbol{\omega} \right)|_{\partial T} \in L^2(\partial T) \right\}$$

The symmetric DG Trefftz formulation

A Green formula on one element T :

$$\int_T (\nabla \times \frac{1}{\mu_T} \nabla \times \mathbf{E}) \cdot \boldsymbol{\omega} dx = \int_T (\frac{1}{\mu_T} \nabla \times \mathbf{E}) \cdot (\nabla \times \boldsymbol{\omega}) dx + \int_{\partial T} \mathbf{n} \times (\frac{1}{\mu_T} \nabla \times \mathbf{E})|_{\partial\Omega} \cdot \boldsymbol{\omega} ds$$

The symmetric DG Trefftz formulation

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Replace $\nabla \times \frac{1}{\mu} \nabla \times \mathbf{E}$ by $\varepsilon k_T^2 \mathbf{E}$ and sum over Trefftz elements:

The symmetric DG Trefftz formulation

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Replace $\nabla \times \frac{1}{\mu} \nabla \times \mathbf{E}$ by $\varepsilon k_T^2 \mathbf{E}$ and sum over Trefftz elements:

$$\sum_{T \in \mathcal{T}} \int_T \left(\frac{1}{\mu} (\nabla \times \mathbf{E}) \cdot (\nabla \times \boldsymbol{\omega}) - \varepsilon k_T^2 \mathbf{E} \cdot \boldsymbol{\omega} \right) dx = \sum_{T \in \mathcal{T}} \int_{\partial T} (\frac{1}{\mu} \nabla \times \mathbf{E})|_{\partial T} \cdot \mathbf{n}_T \times \boldsymbol{\omega}_T ds$$

The symmetric DG Trefftz formulation

A Green formula on one element T :

$$\int_T (\nabla \times \frac{1}{\mu_T} \nabla \times \mathbf{E}) \cdot \boldsymbol{\omega} dx = \int_T (\frac{1}{\mu_T} \nabla \times \mathbf{E}) \cdot (\nabla \times \boldsymbol{\omega}) dx + \int_{\partial T} \mathbf{n} \times (\frac{1}{\mu_T} \nabla \times \mathbf{E})|_{\partial\Omega} \cdot \boldsymbol{\omega} ds$$

Replace $\nabla \times \frac{1}{\mu} \nabla \times \mathbf{E}$ by $\varepsilon k_T^2 \mathbf{E}$ and sum over Trefftz elements:

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The symmetric DG Trefftz formulation

We can invert the roles of \mathbf{E} and $\boldsymbol{\omega}$ because $\boldsymbol{\omega}$ verifies Maxwell on each element:

$$\sum_{T \in \mathcal{T}} \int_T \left(\frac{1}{\mu} (\nabla \times \mathbf{E}) \cdot (\nabla \times \boldsymbol{\omega}) - \varepsilon k_T^2 \mathbf{E} \cdot \boldsymbol{\omega} \right) dx = \sum_{T \in \mathcal{T}} \int_{\partial T} \left(\frac{1}{\mu} \nabla \times \boldsymbol{\omega} \right) |_{\partial T} \cdot \mathbf{n}_T \times \mathbf{E}_T ds$$

Compute difference:

$$\sum_{T \in \mathcal{T}} \int_{\partial T} \left(\left(\frac{1}{\mu} \nabla \times \mathbf{E} \right) |_{\partial T} \cdot \mathbf{n}_T \times \boldsymbol{\omega}_T - \left(\frac{1}{\mu} \nabla \times \boldsymbol{\omega} \right) |_{\partial T} \cdot \mathbf{n}_T \times \mathbf{E}_T \right) ds = 0.$$

The symmetric DG Trefftz formulation

Notation: sums and differences on edges

On an edge $F = \partial T \cap \partial K$ we define

The trace jump: $[[\omega]] = \mathbf{n}_T \times \omega_T + \mathbf{n}_K \times \omega_K.$

The trace average: $\{\{\omega\}\} = \frac{1}{2}(\omega_T + \omega_K).$

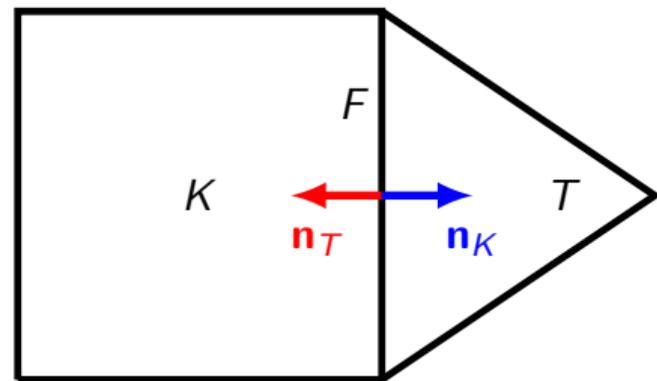


Figure: Schematic view over two neighbouring Trefftz elements sharing a common edge F with normals.

The symmetric DG Trefftz formulation

The variational formulation

$$\begin{cases} \mathbf{E} \in X_T, \forall \omega \in X_T \\ a(\mathbf{E}, \omega) = L\omega \end{cases}$$

The symmetric DG Trefftz formulation

The variational formulation

$$\left\{ \begin{array}{l} \mathbf{E} \in X_T, \forall \omega \in X_T \\ a(\mathbf{E}, \omega) = L\omega \end{array} \right.$$

$$\begin{aligned} & \int_{\Gamma} \{ \{ \mathbf{E} \} \} \cdot \left[\left[\frac{1}{\mu} \nabla \times \omega \right] \right] + \left[\left[\frac{1}{\mu} \nabla \times \mathbf{E} \right] \right] \cdot \{ \{ \omega \} \} \\ & - \{ \{ \frac{1}{\mu} \nabla \times \mathbf{E} \} \} \cdot \left[\left[\omega \right] \right] - \left[\left[\mathbf{E} \right] \right] \cdot \{ \{ \frac{1}{\mu} \nabla \times \omega \} \} ds \\ & + \int_{\partial\Omega} \mathbf{E} \cdot \mathbf{n} \times \left(\frac{1}{\mu} \nabla \times \omega \right) + \mathbf{n} \times \left(\frac{1}{\mu} \nabla \times \mathbf{E} \right) \cdot \omega ds \\ & - 2 \int_{\partial\Omega_R} \frac{1}{Z} \left(\frac{1}{\mu} \nabla \times \mathbf{E} \right) \cdot \left(\frac{1}{\mu} \nabla \times \omega \right) ds \end{aligned}$$

The symmetric DG Trefftz formulation

The variational formulation

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$$\begin{aligned} & \int_{\Gamma} \{ \{ \mathbf{E} \} \} \cdot \left[\left[\frac{1}{\mu} \nabla \times \boldsymbol{\omega} \right] \right] + \left[\left[\frac{1}{\mu} \nabla \times \mathbf{E} \right] \right] \cdot \{ \{ \boldsymbol{\omega} \} \} \\ & - \{ \{ \frac{1}{\mu} \nabla \times \mathbf{E} \} \} \cdot \left[\left[\boldsymbol{\omega} \right] \right] - \left[\left[\mathbf{E} \right] \right] \cdot \{ \{ \frac{1}{\mu} \nabla \times \boldsymbol{\omega} \} \} ds \\ & + \int_{\partial\Omega} \mathbf{E} \cdot \mathbf{n} \times \left(\frac{1}{\mu} \nabla \times \boldsymbol{\omega} \right) + \mathbf{n} \times \left(\frac{1}{\mu} \nabla \times \mathbf{E} \right) \cdot \boldsymbol{\omega} ds \\ & - 2 \int_{\partial\Omega_R} \frac{1}{Z} \left(\frac{1}{\mu} \nabla \times \mathbf{E} \right) \cdot \left(\frac{1}{\mu} \nabla \times \boldsymbol{\omega} \right) ds \\ & = -2 \int_{\partial\Omega_R} \frac{1}{Z} \mathbf{g}_R \cdot \left(\frac{1}{\mu} \nabla \times \boldsymbol{\omega} \right) ds + 2 \int_{\partial\Omega_D} \mathbf{g}_D \cdot \mathbf{n} \times \left(\frac{1}{\mu} \nabla \times \boldsymbol{\omega} \right) ds. \end{aligned}$$

The symmetric DG Trefftz formulation

The local problem: an isomorphism

$$\left\{ \begin{array}{ll} \nabla \times \frac{1}{\mu_T} \nabla \times \boldsymbol{\omega}_g - \varepsilon_T k_T^2 \boldsymbol{\omega}_g = 0 & \text{in } T \\ \mathbf{n} \times \left(\frac{1}{\mu_T} \nabla \times \boldsymbol{\omega}_g \right) - Z_T \mathbf{n} \times (\boldsymbol{\omega}_g \times \mathbf{n}) = \mathbf{g} & \text{on } \partial T \end{array} \right.$$

Solved with impedance BC

$$\mathcal{L} : L^2(\partial T) \rightarrow X_T$$

$$\mathbf{g} \mapsto \mathcal{L}(\mathbf{g}) = \boldsymbol{\omega}_g$$

The symmetric DG Trefftz formulation

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Solved with impedance BC

$\text{Im}(Z_T) > 0$, example:

$$Z_T = i\sqrt{\mu_T \varepsilon_T} k$$

The symmetric DG Trefftz formulation

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Well posed.

The symmetric DG Trefftz formulation

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$\text{Im}(Z_T) > 0$, example:

$$Z_T = i\sqrt{\mu_T \varepsilon_T} k$$

Well posed.

Direct access to curl trace.

The symmetric DG Trefftz formulation

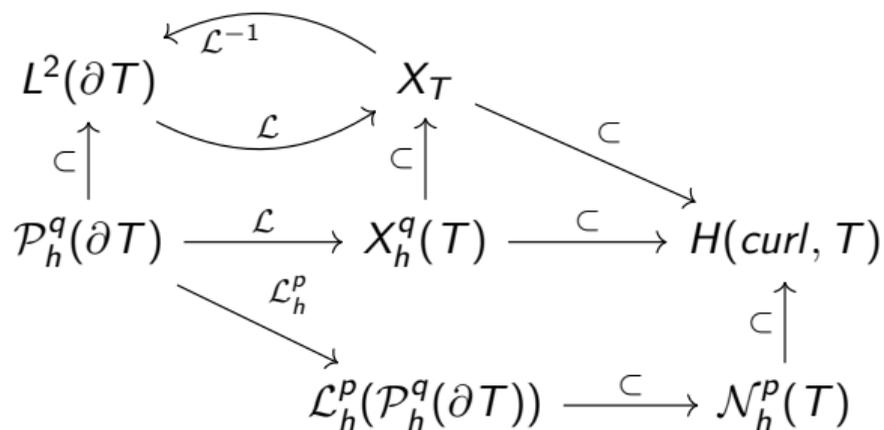


Figure: Relationship between all relevant function spaces. Arrows with \subset denote inclusion maps.

The symmetric DG Trefftz formulation

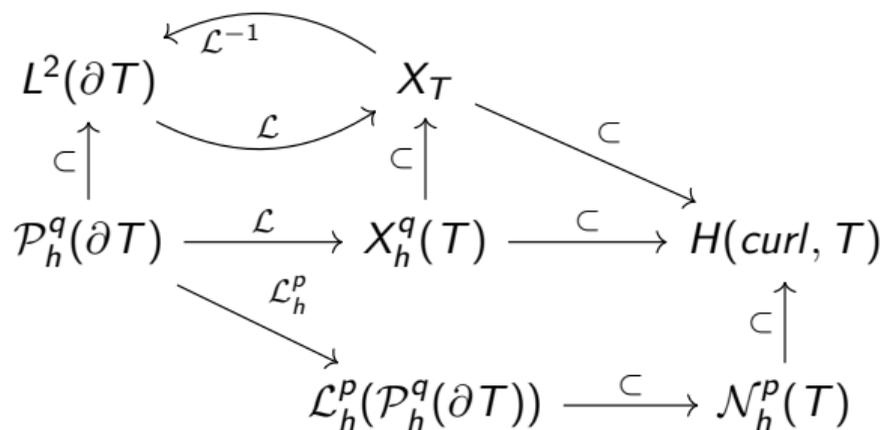


Figure: Relationship between all relevant function spaces. Arrows with \subset denote inclusion maps.

Approximation of impedance boundary condition:

$$\mathcal{P}_h^q(\partial T) := \{\mathbf{g} \in L^2(\partial T), \quad \mathbf{g}|_f \in \mathcal{P}^q(f), \quad \forall f, \quad f \in \mathcal{F}_{\partial T}^h\}$$

The symmetric DG Trefftz formulation

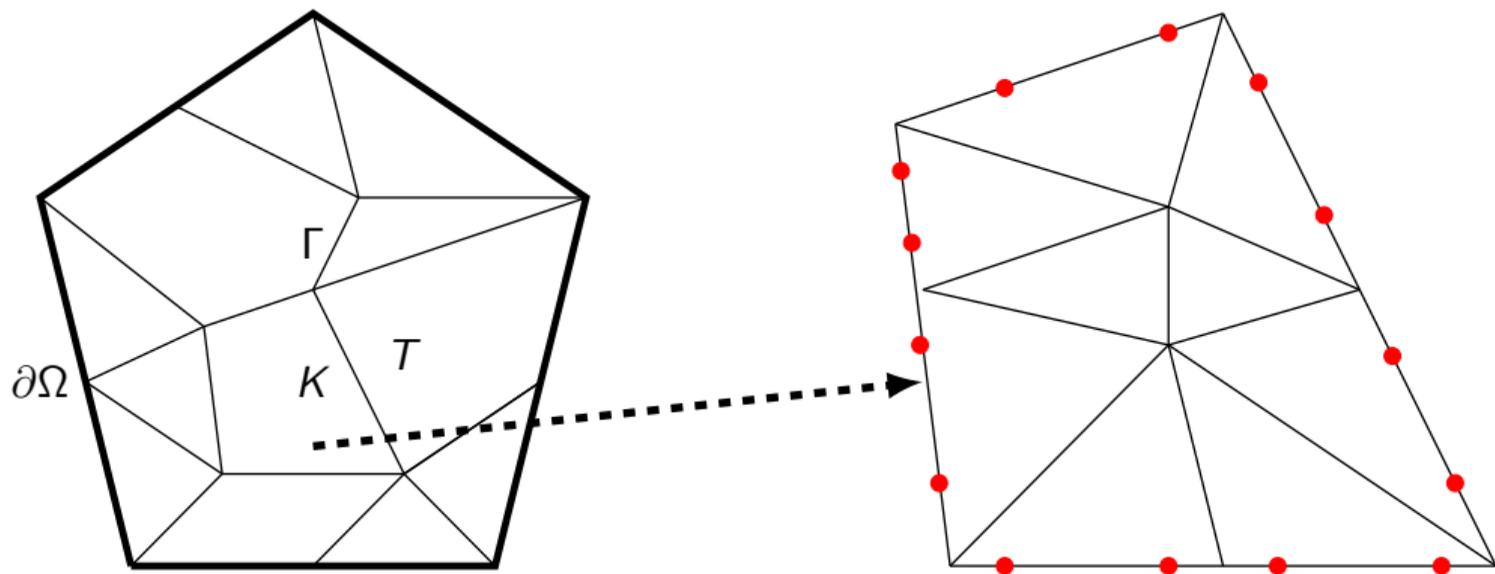


Figure: To the left: the Trefftz DG mesh. Γ is the interior edges. K and T are two neighbouring Trefftz elements. To the right: one Trefftz element with a triangular FE mesh.

Approximation of the local problem: Nedelec finite element method

The weak formulation:

$$\left\{ \begin{array}{l} \mathbf{E} \in H_0(\text{curl}, \Omega), \forall \boldsymbol{\omega} \in H_0(\text{curl}, \Omega) \\ \int_{\Omega} \left(\frac{1}{\mu} \nabla \times \mathbf{E} \right) \cdot (\nabla \times \boldsymbol{\omega}) dx - k^2 \int_{\Omega} \varepsilon \mathbf{E} \cdot \boldsymbol{\omega} dx \\ \quad + Z \int_{\partial\Omega_R} \mathbf{n} \times (\mathbf{E} \times \mathbf{n}) \cdot \boldsymbol{\omega} ds = - \int_{\partial\Omega_R} \mathbf{g} \cdot \boldsymbol{\omega} ds \end{array} \right.$$

Inhomogenous Dirichlet data is treated with a variable change.

Approximation of the local problem: Nedelec finite element method

Validation of method

$$\mathbf{k} = k \begin{bmatrix} \cos(\theta) \\ \sin(\theta) \end{bmatrix}, \quad \mathbf{E} = E \begin{bmatrix} -\sin(\theta) \\ \cos(\theta) \end{bmatrix} e^{-i\mathbf{k}\mathbf{x}}$$

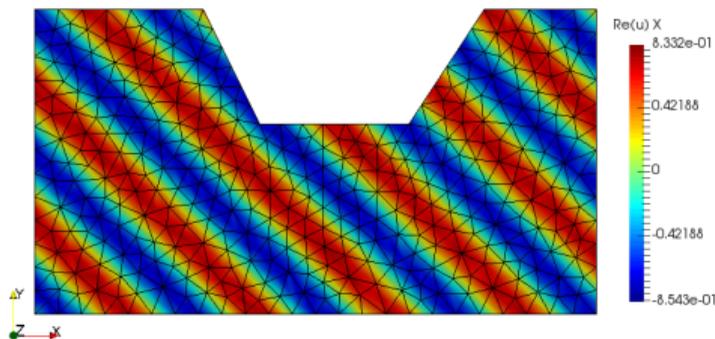


Figure: A plane wave test: $\theta = 45$ degrees.
 $\rho = 1, h = 0.13, k = 4\pi$.

Approximation of the local problem: Nedelec finite element method

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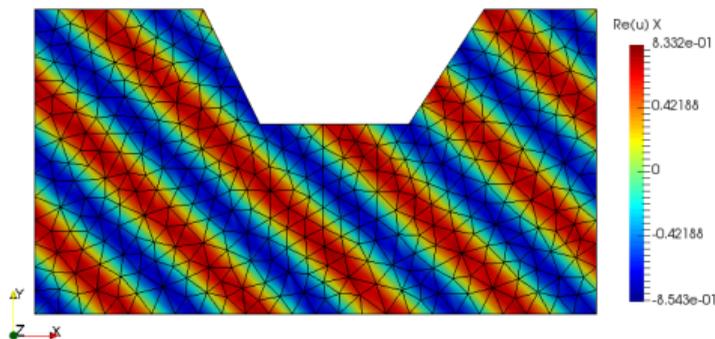


Figure: A plane wave test: $\theta = 45$ degrees.
 $p = 1, h = 0.13, k = 4\pi$.

$$\|\cdot\|_{H^1(\text{curl})} = \sqrt{\int_{\Omega} |\cdot|^2 dx + \int_{\Omega} \frac{1}{k^2} |\nabla \times \cdot|^2 dx}$$

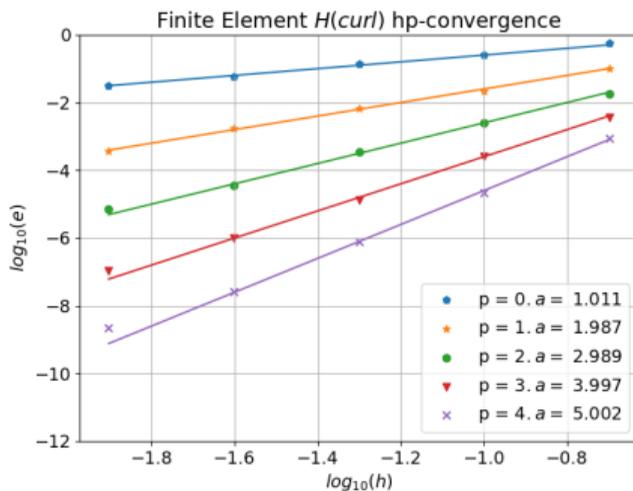
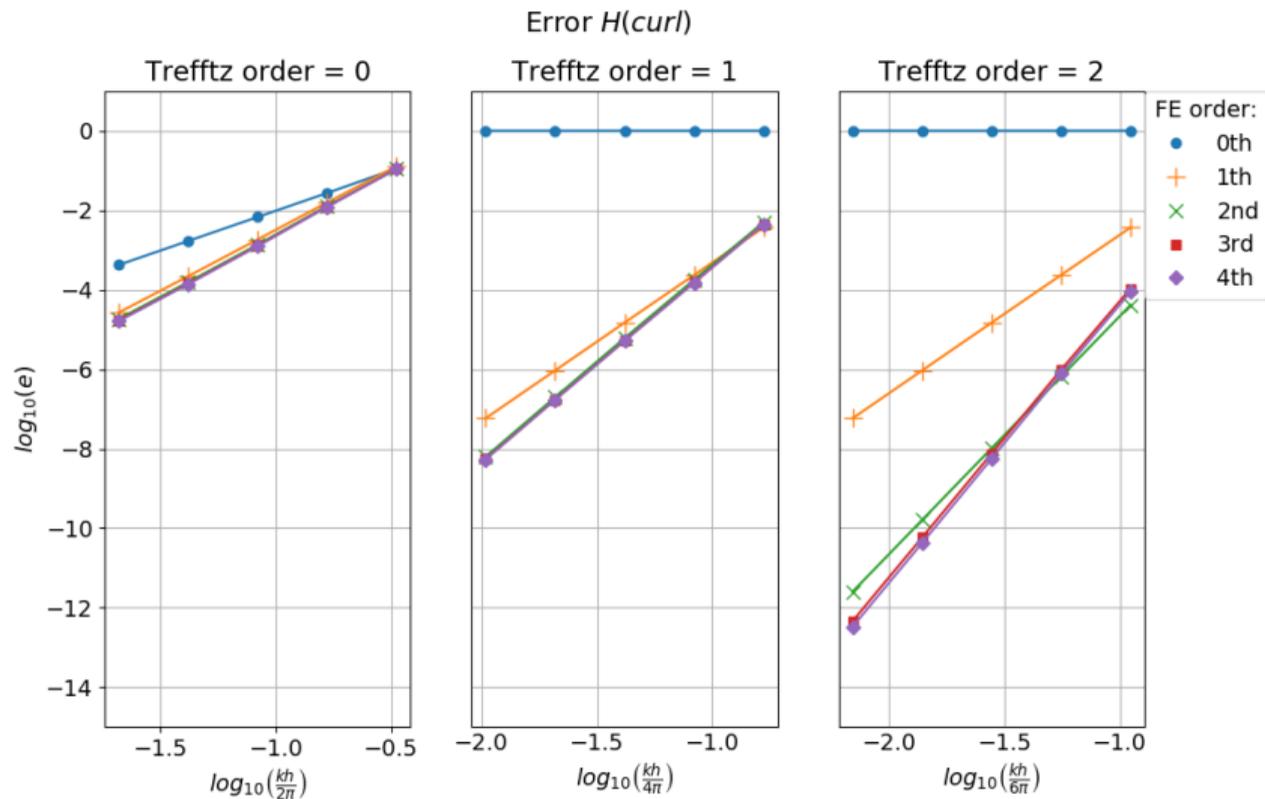


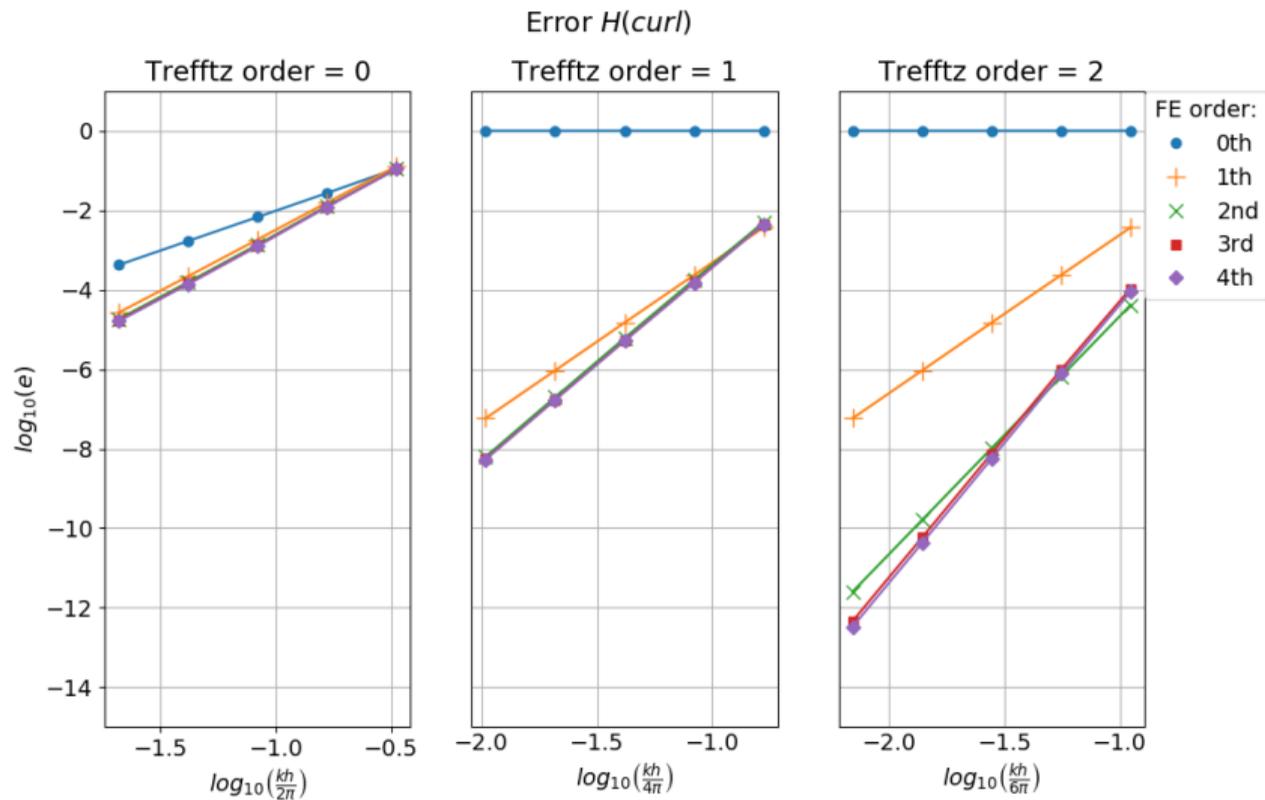
Figure: Relative error convergence rate:
 $e = Ch^{p+1}$

Approximation of the local problem: Nedelec finite element method



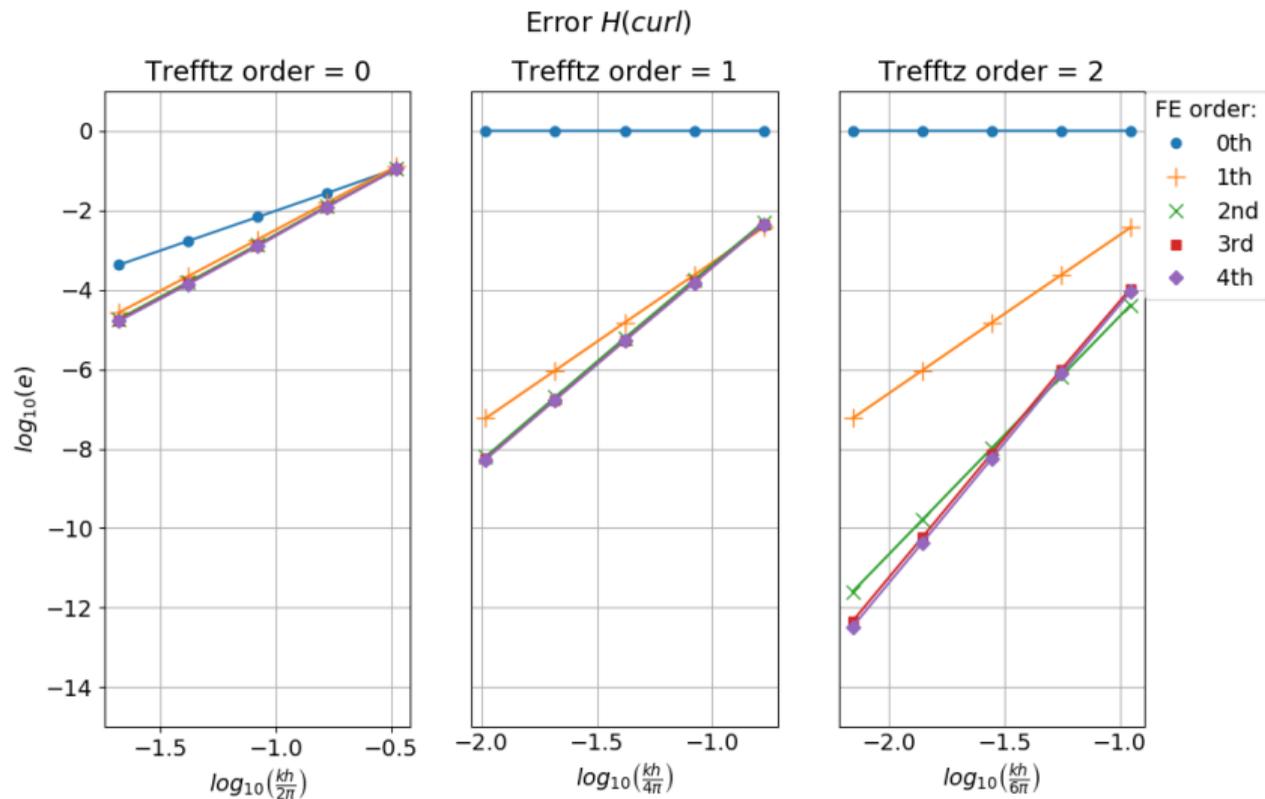
Rule of thumb: $p \geq q$

Approximation of the local problem: Nedelec finite element method



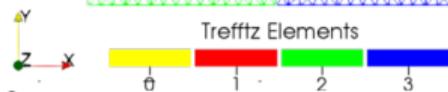
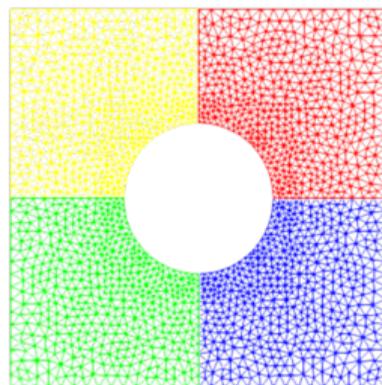
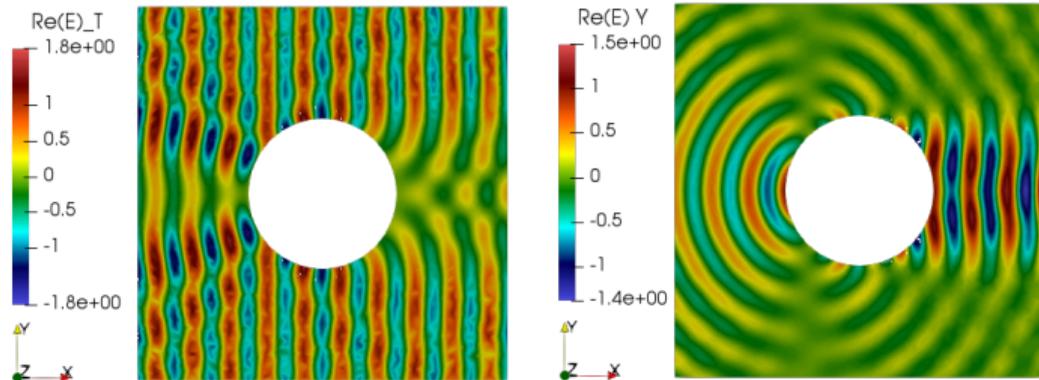
Rule of thumb: $p \geq q$
 $p < q \rightarrow$ precision loss

Approximation of the local problem: Nedelec finite element method



Rule of thumb: $p \geq q$
 $p < q \rightarrow$ precision loss
Super convergence

A qualitative result: scattering on a perfect conducting circle



$$\mathbf{E}_{total} = \mathbf{E}_{incident} + \mathbf{E}_{scatter}$$

Incident plane wave from the left

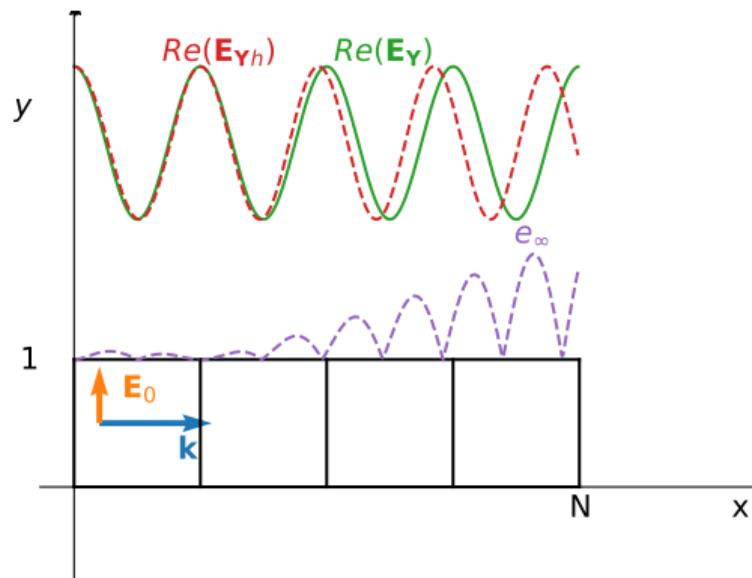
On the left: \mathbf{E}_{total}

On the right: $\mathbf{E}_{scatter}$

Long range propagation: Numerical dispersion

$$\left\{ \begin{array}{l} \nabla \times \nabla \times \mathbf{E} - k^2 \mathbf{E} = 0 \quad \text{in } \Omega = [0, L] \times [0, 1] \\ \mathbf{n} \times (\mathbf{E} \times \mathbf{n}) = 0, \quad y \in \{0, 1\} \\ \mathbf{n} \times (\mathbf{E} \times \mathbf{n}) = -e_y, \quad x = 0 \\ \mathbf{n} \times \left(\frac{1}{\mu} \nabla \times \mathbf{E} \right) - ik \mathbf{n} \times (\mathbf{E} \times \mathbf{n}) = 0, \quad x = L \end{array} \right.$$

$$e_\infty = 100 \max_{(x,y) \in \Omega} \frac{|\mathbf{E} - \mathbf{E}_h|}{\|\mathbf{E}\|_\infty}.$$



Long range propagation: Numerical dispersion

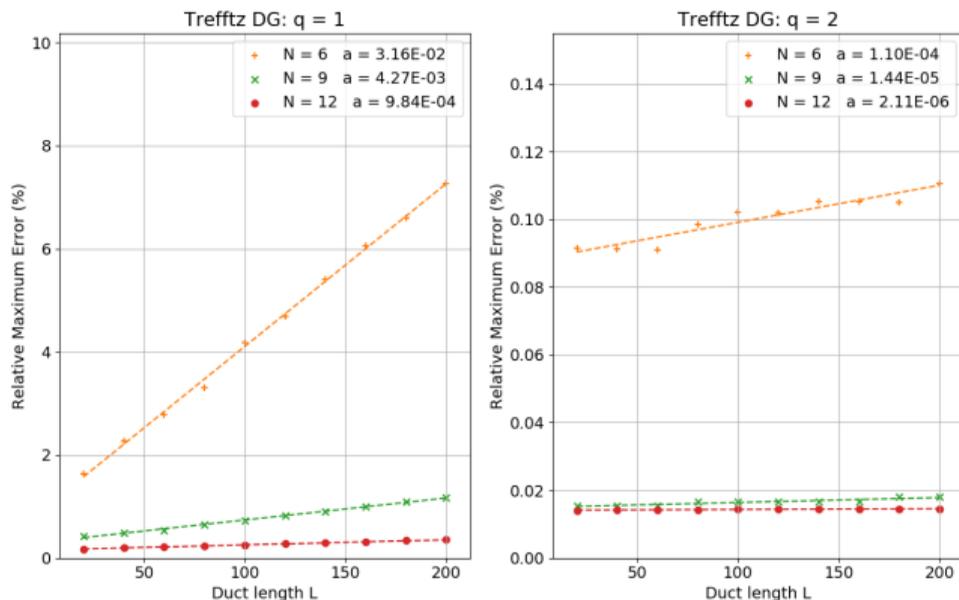


Figure: Relative maximum order for long range propagation using the FE method for different orders and meshes. N on this figure corresponds to $1/h$.

Long range propagation: Numerical dispersion

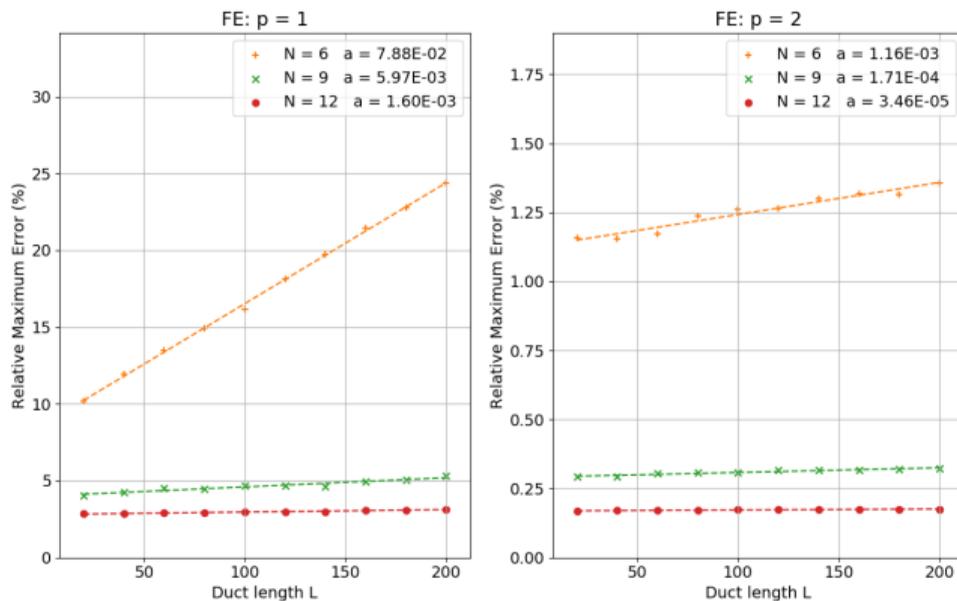
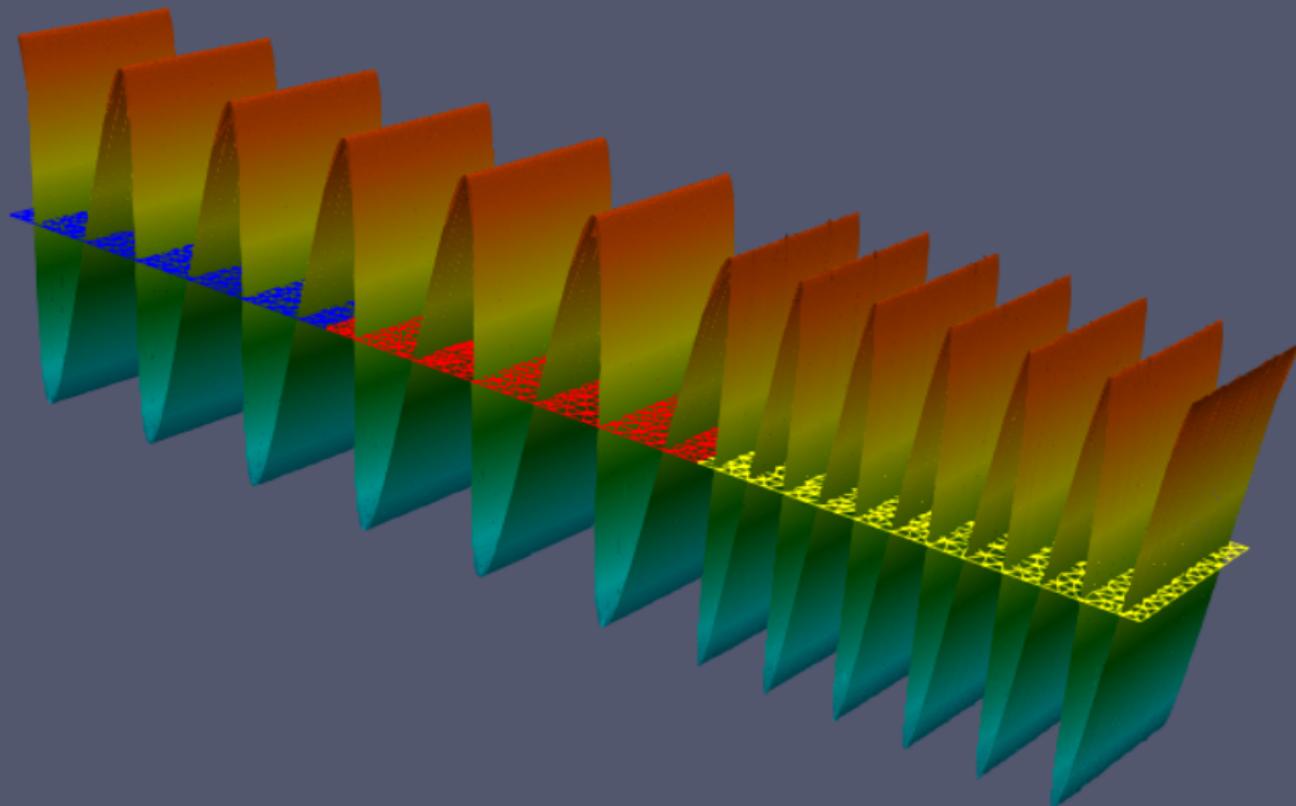
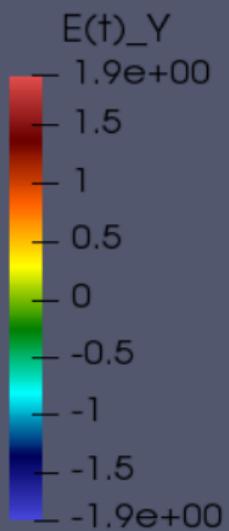
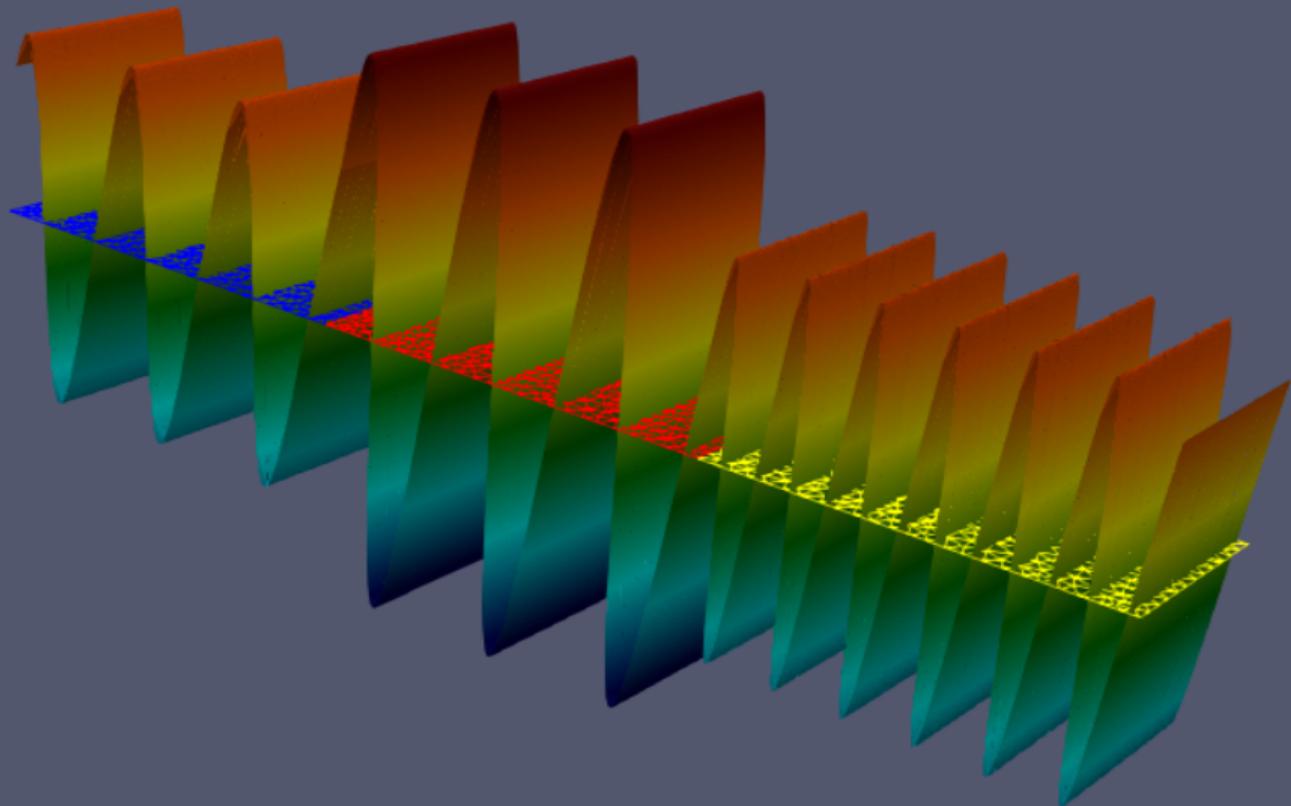
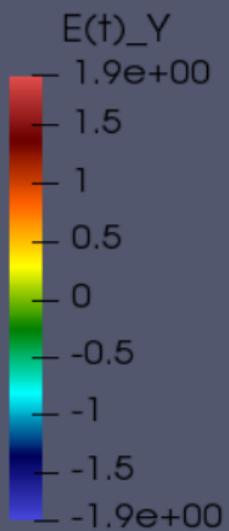


Figure: Relative maximum order for long range propagation using the FE method for different orders and meshes.



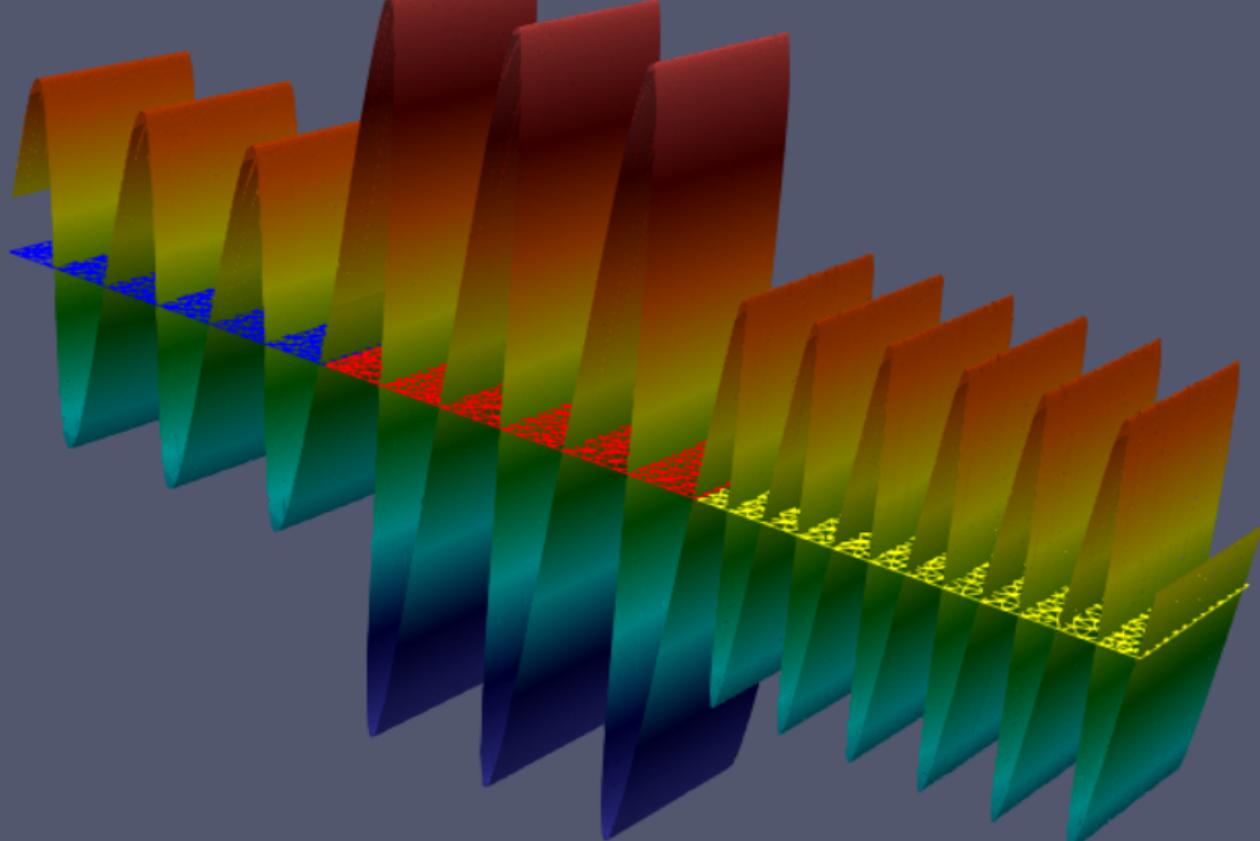
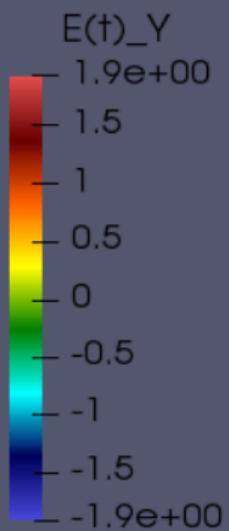
Trefftz elements





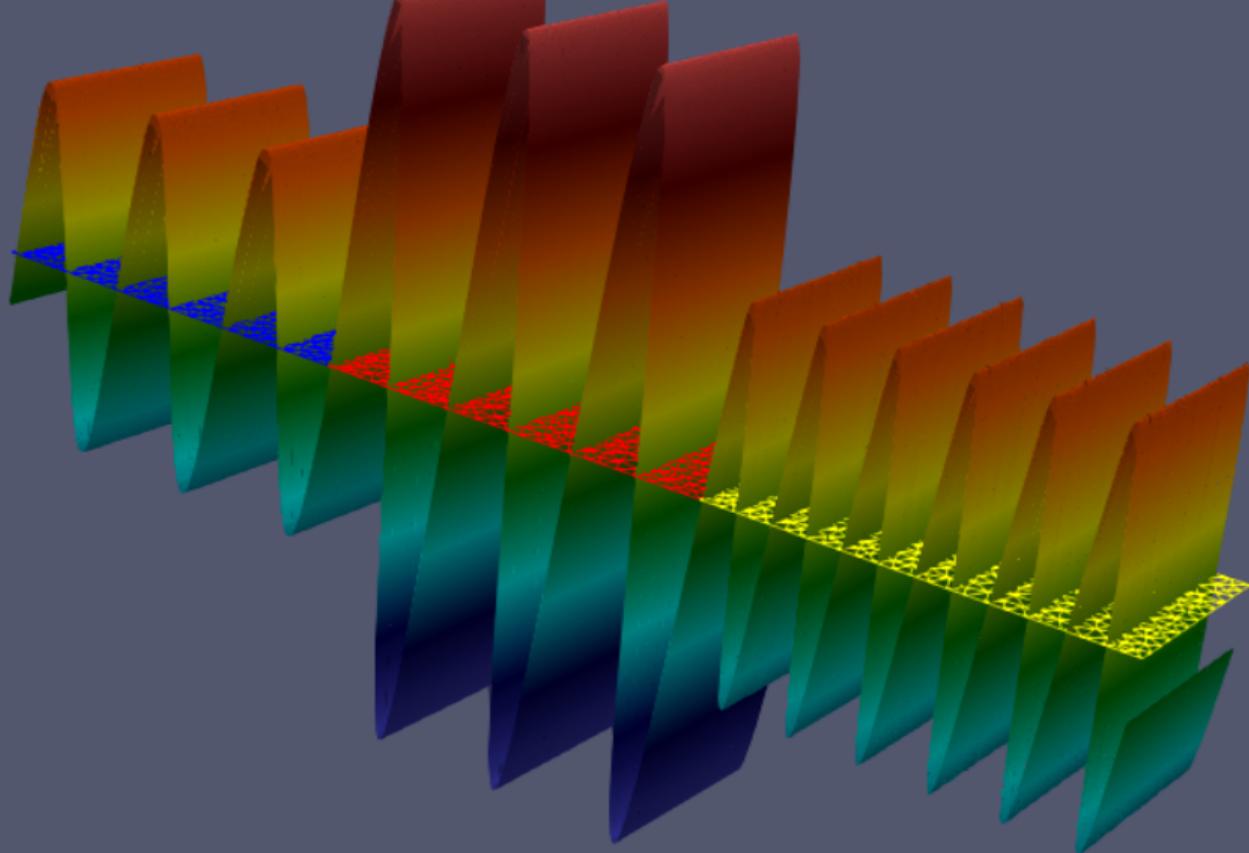
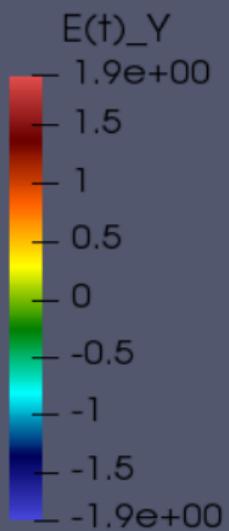
Trefftz elements





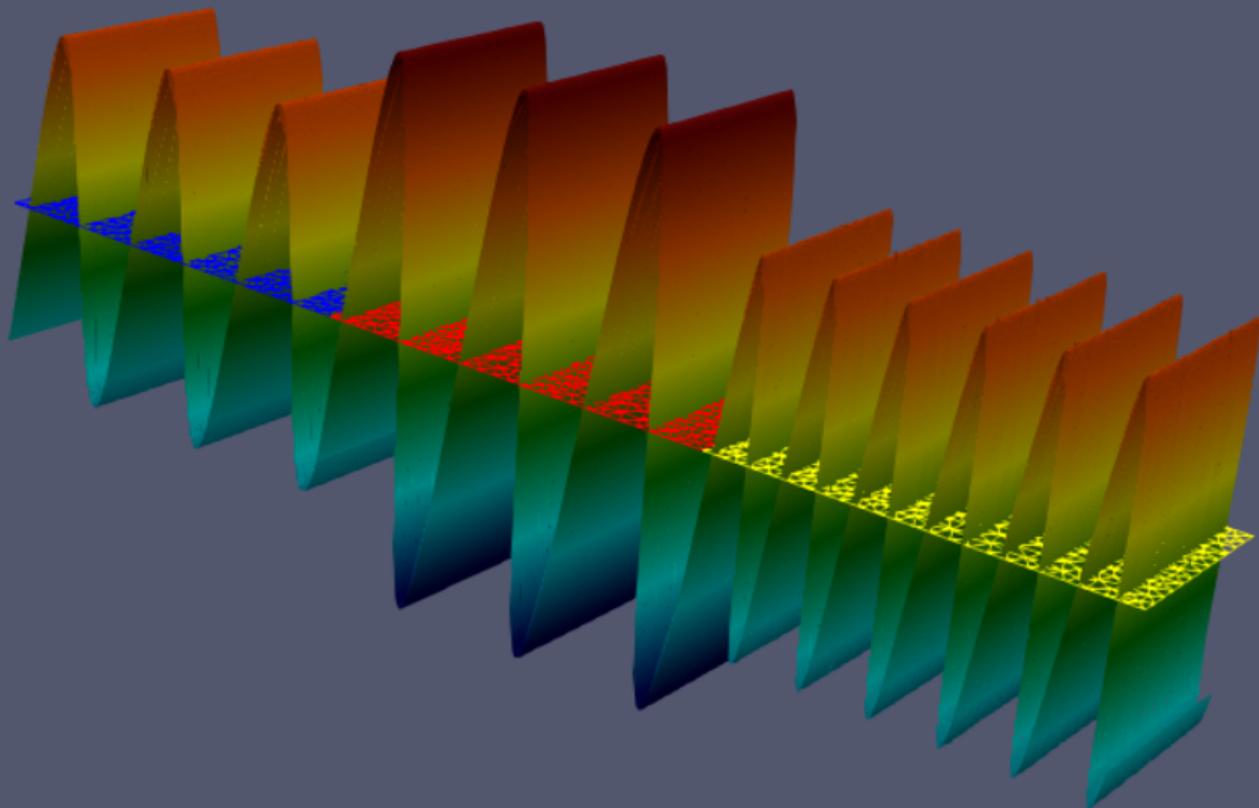
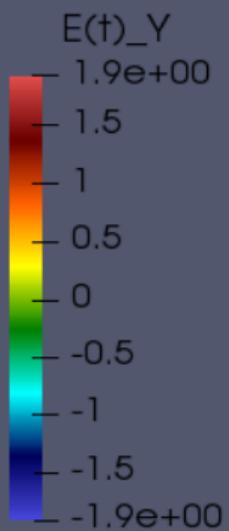
Trefftz elements





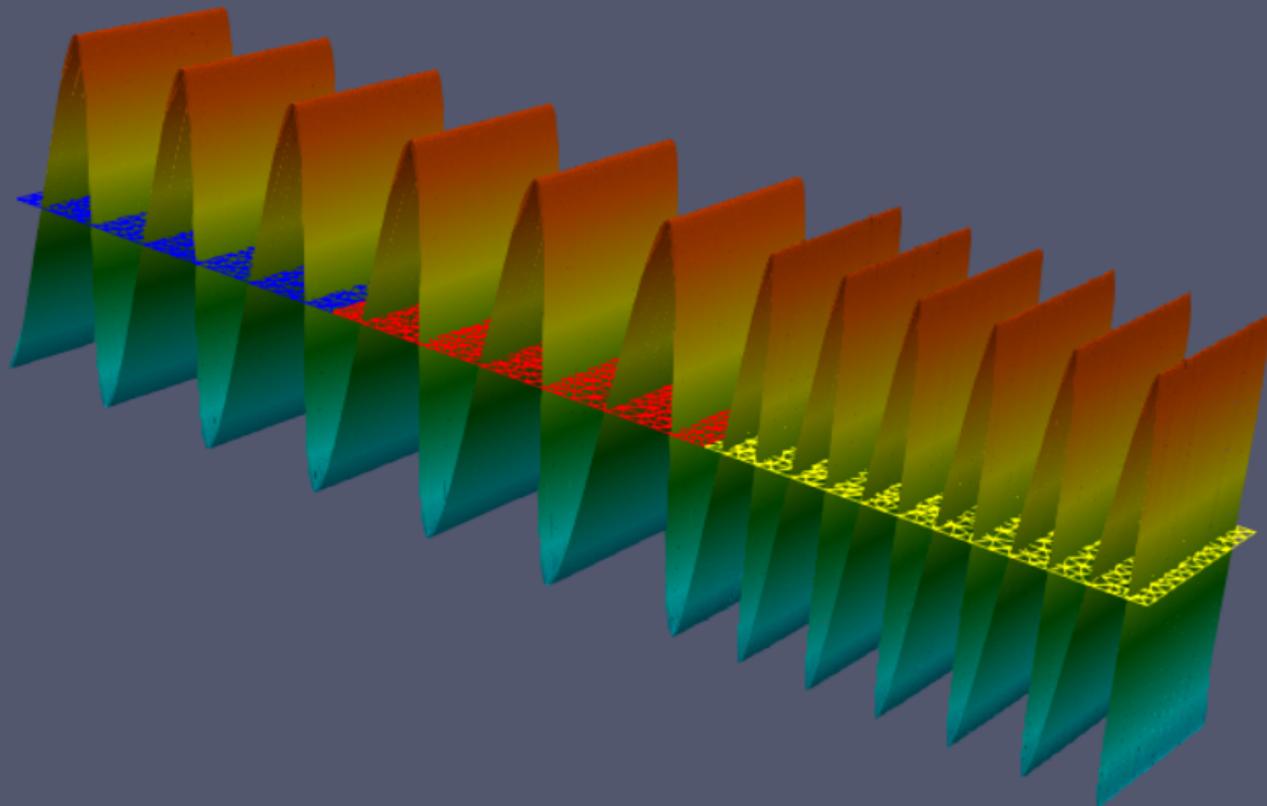
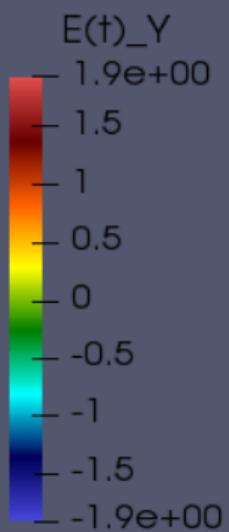
Trefftz elements





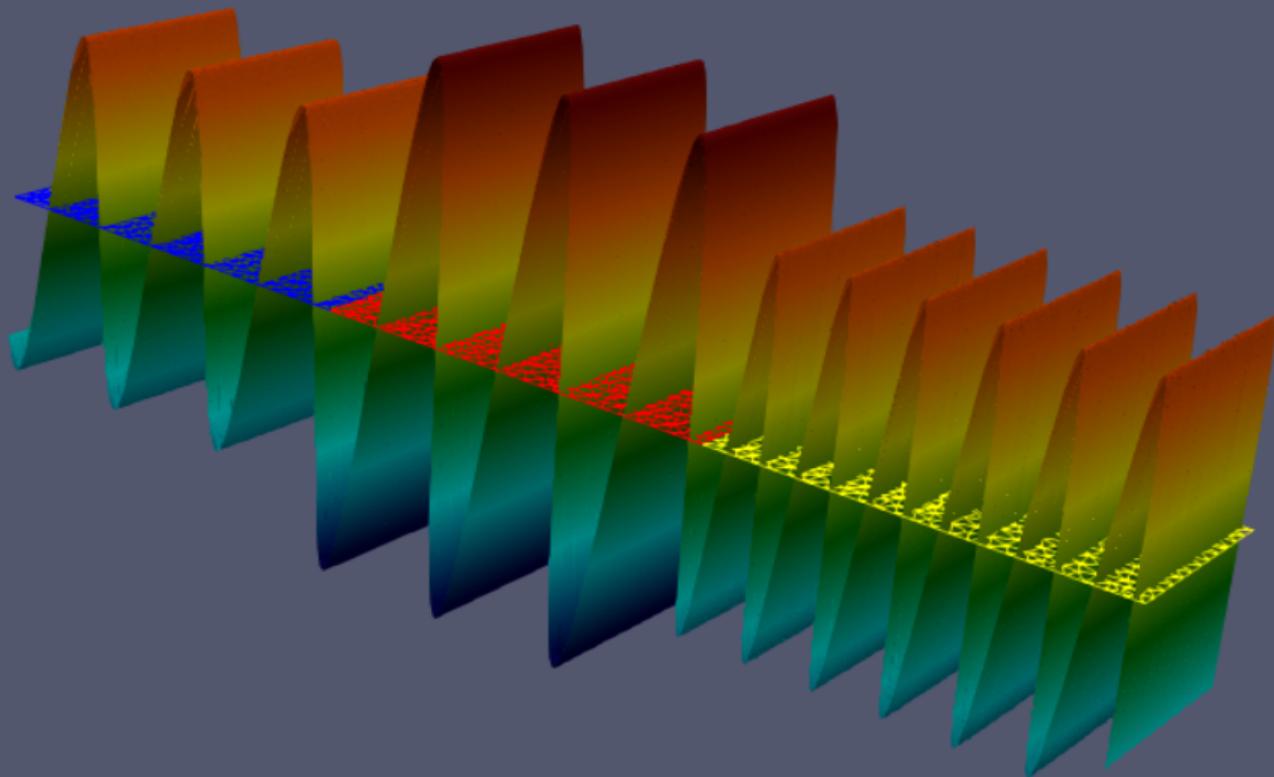
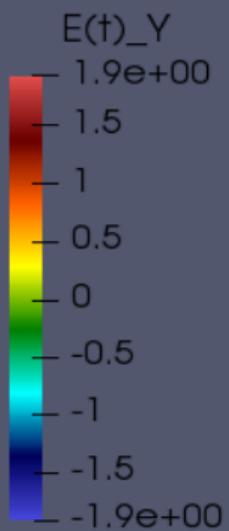
Trefftz elements





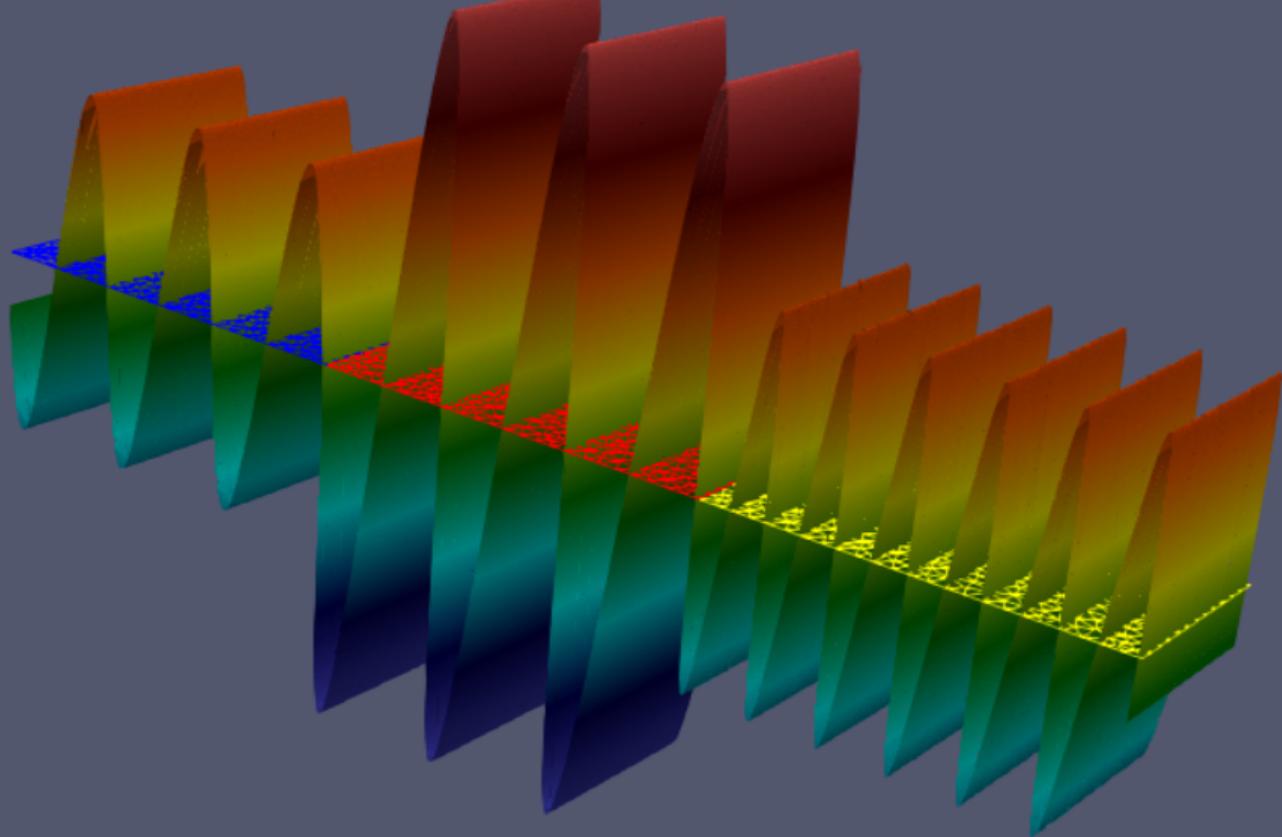
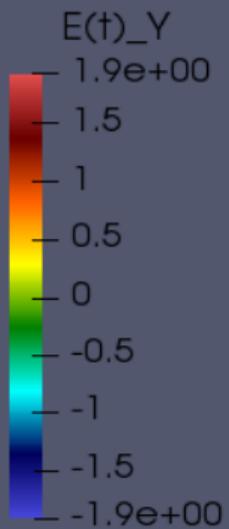
Trefftz elements





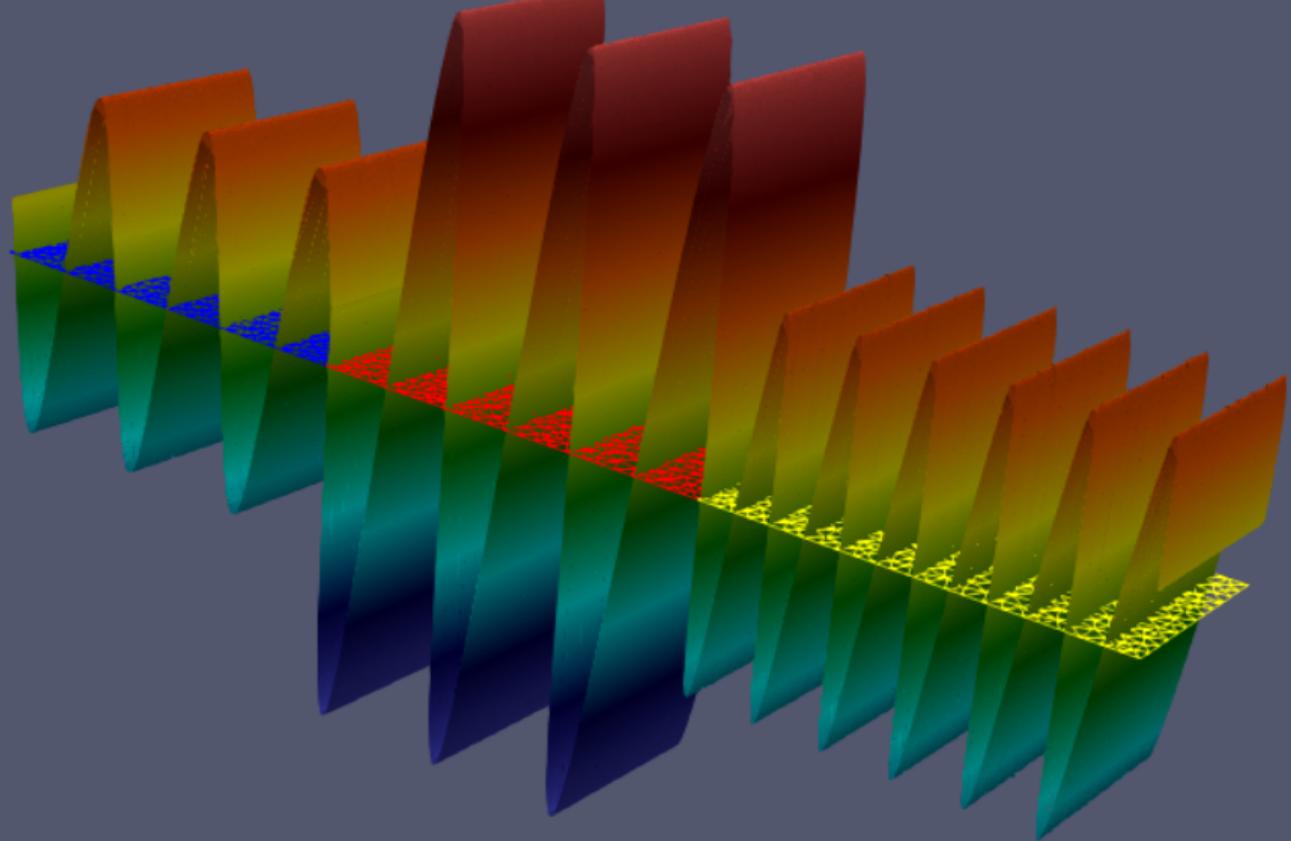
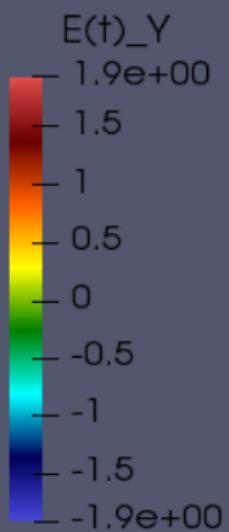
Trefftz elements





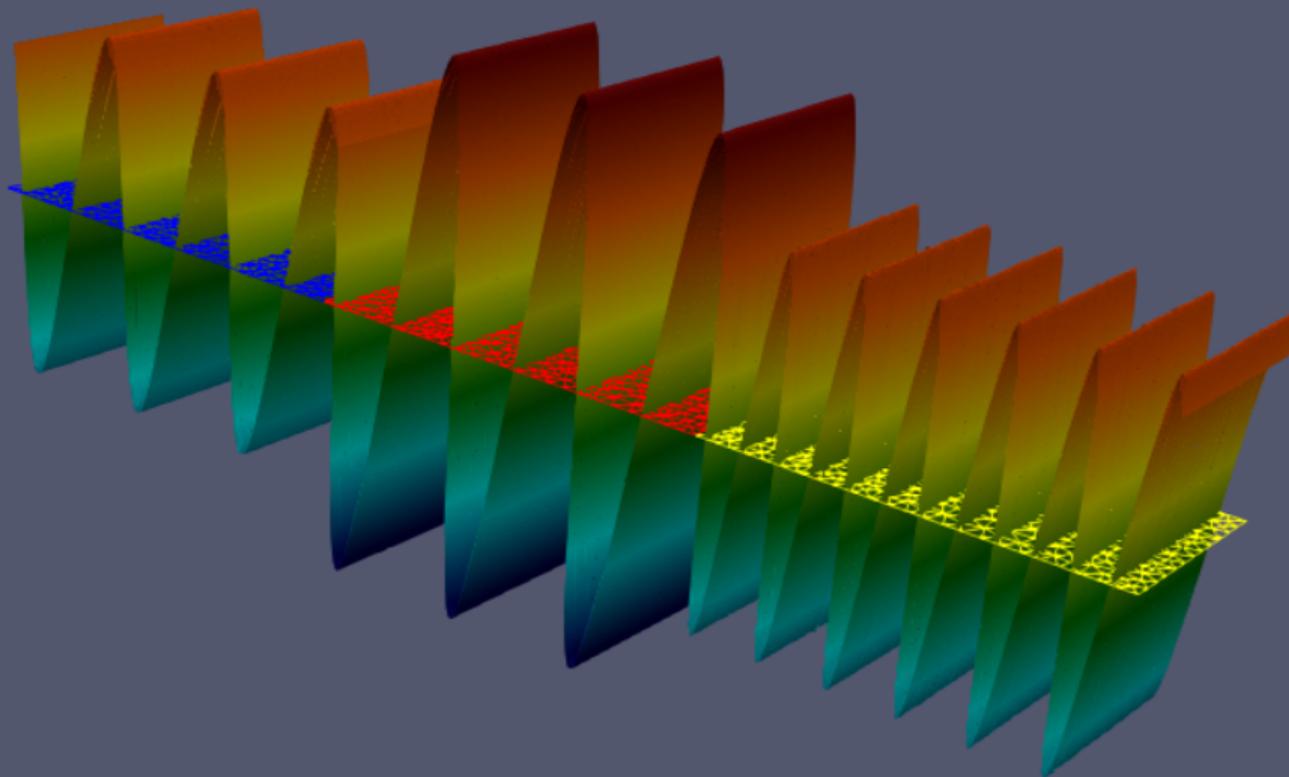
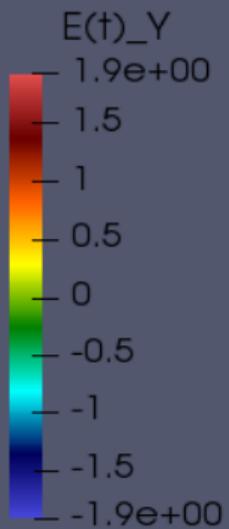
Trefftz elements





Trefftz elements





Trefftz elements



Conclusion and perspectives

Trefftz IPDG formulation combined with BEM reduces the pollution effect
FEM UWVF shows the same properties. We have only very preliminary results
that can not be yet presented

The future: extension to elastic waves. Not that obvious when considering BEM
or FEM...

With Sébastien Pernet, we are planning to answer to call to get a PhD thesis.